

มาตรฐานผลิตภัณฑ์อุตสาหกรรม

THAI INDUSTRIAL STANDARD

มอก. 1340 – 2550

ISO 5657 : 1997

**ปฏิกิริยาต่อการทดสอบความทนไฟ -  
ความสามารถในการติดไฟของวัสดุก่อสร้างโดยใช้  
แหล่งกำเนิดความร้อนแบบแผ่รังสี**

REACTION TO FIRE TESTS - IGNITABILITY OF BUILDING PRODUCTS USING  
A RADIANT HEAT SOURCE

สำนักงานมาตรฐานผลิตภัณฑ์อุตสาหกรรม

กระทรวงอุตสาหกรรม

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มาตรฐานผลิตภัณฑ์อุตสาหกรรม  
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กระทรวงอุตสาหกรรม ถนนพระรามที่ 6 กรุงเทพฯ 10400  
โทรศัพท์ 02 202 3300

ประกาศในราชกิจจานุเบกษาฉบับประกาศและงานทั่วไปเล่ม 124 ตอนพิเศษ 200ง  
วันที่ 21 ธันวาคม พุทธศักราช 2550

มาตรฐานผลิตภัณฑ์อุตสาหกรรม ปฏิบัติการทดสอบความทนไฟ - ความสามารถในการติดไฟของวัสดุก่อสร้าง โดยใช้แหล่งกำเนิดความร้อนแบบแผ่รังสี นี้ได้ประกาศใช้ครั้งแรกเป็นมาตรฐานผลิตภัณฑ์อุตสาหกรรม การทดสอบความทนไฟ- ปฏิบัติการต่อไฟ-ความสามารถในการติดไฟของวัสดุก่อสร้าง มาตรฐานเลขที่ มอก.1340-2539 ในราชกิจจานุเบกษา ฉบับประกาศทั่วไป เล่ม 113 ตอนที่ 51 ง วันที่ 25 มิถุนายน พุทธศักราช 2539 ต่อมาได้พิจารณาเห็นสมควรแก้ไขปรับปรุงเพื่อให้สอดคล้องกับเอกสารอ้างอิง จึงได้แก้ไขปรับปรุงโดยยกเลิกมาตรฐานเดิมและกำหนดมาตรฐานนี้ขึ้นใหม่

มาตรฐานผลิตภัณฑ์อุตสาหกรรมนี้กำหนดขึ้นโดยรับโดยการรับ ISO 5657 : 1997 Reaction to fire tests Ignitability of building products using a radiant heat source มาใช้ในระดับเหมือนกันทุกประการ (identical) โดยใช้ ISO ฉบับภาษาอังกฤษเป็นหลัก

มาตรฐานผลิตภัณฑ์อุตสาหกรรมนี้กำหนดขึ้นเพื่อให้ทันกับความต้องการของผู้ใช้และจักได้แปลเป็นภาษาไทยในโอกาสอันสมควร หากมีข้อสงสัยโปรดติดต่อสอบถามที่สำนักงานมาตรฐานผลิตภัณฑ์อุตสาหกรรม

คณะกรรมการมาตรฐานผลิตภัณฑ์อุตสาหกรรมได้พิจารณามาตรฐานนี้แล้ว เห็นสมควรเสนอรัฐมนตรีประกาศตาม มาตรา 15 แห่งพระราชบัญญัติมาตรฐานผลิตภัณฑ์อุตสาหกรรม พ.ศ. 2511



## ประกาศกระทรวงอุตสาหกรรม

ฉบับที่ 3788 (พ.ศ. 2550)

ออกตามความในพระราชบัญญัติมาตรฐานผลิตภัณฑ์อุตสาหกรรม

พ.ศ. 2511

เรื่อง ยกเลิกมาตรฐานผลิตภัณฑ์อุตสาหกรรม

การทดสอบความทนไฟ-ปฏิกิริยาต่อไฟ-ความสามารถในการติดไฟของวัสดุก่อสร้าง

และกำหนดมาตรฐานผลิตภัณฑ์อุตสาหกรรม

ปฏิกิริยาต่อการทดสอบความทนไฟ-ความสามารถในการติดไฟของวัสดุก่อสร้างโดยใช้

แหล่งกำเนิดความร้อนแบบแฟรงก์ลี

โดยที่เป็นการสมควรปรับปรุงมาตรฐานผลิตภัณฑ์อุตสาหกรรม การทดสอบความทนไฟ-ปฏิกิริยาต่อไฟ-ความสามารถในการติดไฟของวัสดุก่อสร้าง มาตรฐานเลขที่ มอก.1340-2539

อาศัยอำนาจตามความในมาตรา 15 แห่งพระราชบัญญัติมาตรฐานผลิตภัณฑ์อุตสาหกรรม พ.ศ. 2511 รัฐมนตรีว่าการกระทรวงอุตสาหกรรมออกประกาศยกเลิกประกาศกระทรวงอุตสาหกรรม ฉบับที่ 2145 (พ.ศ.2539) ออกตามความในพระราชบัญญัติมาตรฐานผลิตภัณฑ์อุตสาหกรรม พ.ศ.2511 เรื่อง กำหนดมาตรฐานผลิตภัณฑ์อุตสาหกรรม การทดสอบความทนไฟ-ปฏิกิริยาต่อไฟ-ความสามารถในการติดไฟของวัสดุก่อสร้าง ลงวันที่ 14 พฤษภาคม พ.ศ.2539 และออกประกาศกำหนดมาตรฐานผลิตภัณฑ์อุตสาหกรรม ปฏิกิริยาต่อการทดสอบความทนไฟ-ความสามารถในการติดไฟของวัสดุก่อสร้างโดยใช้แหล่งกำเนิดความร้อนแบบแฟรงก์ลี มาตรฐานเลขที่ มอก.1340-2550 ขึ้นใหม่ ดังมีรายการละเอียดต่อท้ายประกาศนี้

ทั้งนี้ให้มีผลตั้งแต่วันที่ประกาศในราชกิจจานุเบกษา เป็นต้นไป

ประกาศ ณ วันที่ 12 กันยายน พ.ศ. 2550

โฆสิต ปั้นเปี่ยมรัษฎ์

รัฐมนตรีว่าการกระทรวงอุตสาหกรรม

# มาตรฐานผลิตภัณฑ์อุตสาหกรรม ปฏิกิริยาต่อการทดสอบความทนไฟ - ความสามารถในการติดไฟของวัสดุก่อสร้าง โดยใช้แหล่งกำเนิดความร้อนแบบแผ่รังสี

## บทนำ

มาตรฐานผลิตภัณฑ์อุตสาหกรรมนี้กำหนดขึ้นโดยรับ ISO 5657 : 1997 Reaction to fire tests - Ignitability of building products using a radiant heat source มาใช้ในระดับเหมือนกันทุกประการ (identical) โดยใช้ ISO ฉบับภาษาอังกฤษเป็นหลัก

## ขอบข่าย

มาตรฐานผลิตภัณฑ์อุตสาหกรรมนี้กำหนดวิธีหาคณะลักษณะการติดไฟของพื้นผิวแผ่รังสี ของชิ้นทดสอบ ที่ทำจากวัสดุที่มีผิวราบในตัวเอง ของผสมหรือชุดประกอบที่มีความหนาไม่เกิน 70 มิลลิเมตร เมื่อวางในแนวราบและรับรังสีความร้อนในระดับที่กำหนด

## เอกสารอ้างอิง

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 2

## คำศัพท์และบทนิยาม

ความหมายของคำที่ใช้ในมาตรฐานผลิตภัณฑ์อุตสาหกรรมนี้ให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 3

## หลักการการทดสอบ

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 4

## ลักษณะที่เหมาะสมของผลิตภัณฑ์สำหรับการทดสอบ

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 5

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### **การสร้างและการเตรียมชิ้นทดสอบ**

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 6

### **เครื่องมือทดสอบ**

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 7

### **สภาวะแวดล้อมสำหรับการทดสอบ**

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รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 9

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รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 10

### **วิธีทดสอบ**

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 11

### **การแสดงผล**

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 12

### **รายงานผลทดสอบ**

รายละเอียดให้ขึ้นไปตาม ISO 5657 : 1997 ข้อ 13

**ภาคผนวก ก.**

**ข้อคิดเห็นเกี่ยวกับเนื้อเรื่องและข้อเสนอแนะสำหรับผู้ปฏิบัติงาน**

รายละเอียดให้เป็นไปตาม ISO 5657 : 1997 Annex A

**ภาคผนวก ข.**

**การนำไปใช้งานและข้อจำกัดของการทดสอบ**

รายละเอียดให้เป็นไปตาม ISO 5657 : 1997 Annex B

**ภาคผนวก ค.**

**ความสามารถทางด้านฟลักซ์ความร้อนที่สูงกว่า**

รายละเอียดให้เป็นไปตาม ISO 5657 : 1997 Annex C

**ภาคผนวก ง.**

**การเปรียบเทียบผลระหว่างห้องปฏิบัติการของเวลาในการตัดไฟพื้นผิวอย่างต่อเนื่อง**

รายละเอียดให้เป็นไปตาม ISO 5657 : 1997 Annex D

พจน. 1340-2550  
ISO 5657 : 1997



# Reaction to fire tests — Ignitability of building products using a radiant heat source

**SAFETY WARNING** - So that suitable precautions may be taken to safeguard health, the attention of all concerned in fire tests is drawn to the possibility that toxic or harmful gases may be evolved during exposure of test specimens. The advice on safety given in annex A clause A.7 should also be noted.

## 1 Scope

This International Standard specifies a method for examining the ignition characteristics of the exposed surfaces of specimens of essentially flat materials, composites or assemblies not exceeding 70mm in thickness, when placed horizontally and subjected to specified levels of thermal irradiance.

Annex A gives a commentary on the text and guidance notes for operators. Advice on the limitations of the test is given in annex B.

## 2 Normative references

The following standards contain provisions which, through reference in this text, constitute provisions of this International Standard. At the time of publication, the editions indicated were valid. All standards are subject to revision, and parties to agreements based on this International Standard are encouraged to investigate the possibility of applying the most recent editions of the standards indicated below. Members of IEC and ISO maintain registers of currently valid International Standards.

ISO 291:1997, *Plastics — Standard atmospheres for conditioning and testing*.

ISO/IEC Guide 52:1990, *Glossary of fire terms and definitions*.

ISO/TR 14697:1997, *Reaction to fire tests — Guidance on the choice of substrates for building products*.

## 3 Definitions

NOTE — See also A.1.

For the purposes of this International Standard, the definitions given in ISO/IEC Guide 52, together with the following, apply.

**3.1 assembly:** Fabrication of materials and/or composites.

NOTE – This may include an air gap.

EXAMPLE – Sandwich panels.

**3.2 composite:** Combination of materials which are generally recognised in building construction as discrete entities.

EXAMPLE – Coated or laminated materials.

**3.3 essentially flat surface:** Surface whose irregularity from a plane does not exceed  $\pm 1$  mm.

**3.4 exposed surface:** That surface of the product subjected to the heating conditions of the test.

**3.5 irradiance (at a point of a surface):** Quotient of the radiant flux incident on an infinitesimal element of surface containing the point, by the area of that element.

**3.6 material:** Single substance or uniformly dispersed mixture.

EXAMPLES – Metal, stone, timber, concrete, mineral fibre, polymers.

**3.7 plume ignition:** Inception of any flame in the plume above the specimen, sustained or transitory.

**3.8 product:** Material, composite or assembly about which information is required.

**3.9 specimen:** Representative piece of the product which is to be tested together with any substrate or treatment.

NOTE – This may include an air gap.

**3.10 sustained surface ignition:** Inception of a flame on the surface of the specimen which is still present at the next application of the pilot flame (greater than 4s duration).

**3.11 transitory surface ignition:** Inception of any flame on the surface of the specimen which is not present at the next application of the pilot flame (less than 4s duration).

## 4 Principles of the test

NOTE – See also A.2.

Specimens of the product are mounted horizontally and exposed to thermal radiation on their upper surface at selected levels of constant irradiance within the range 10 to 70kW/m<sup>2</sup>.

A pilot flame is applied at regular intervals to a position 10mm above the centre of each specimen to ignite any volatile gases given off. The time at which sustained surface ignition occurs is reported.

NOTE 1 Information is given on the use of the apparatus to determine the ignitability of materials under higher irradiances in annex C.

NOTE 2 Other types of ignition which occur are reported in 11.5.

NOTE 3 Convection transfer may also make a very small contribution (not more than a few per cent) to the heating at the centre of a specimen and to the reading of the radiometer during the calibration procedure. However, the term irradiance is used throughout this International Standard as best indicating the essentially radiative mode of heat transfer.

## 5 Suitability of a product for testing

NOTE – See also A.3.

### 5.1 Surface characteristics

5.1.1 A product having one of the following properties is suitable for testing:

a) an essentially flat exposed surface; or

b) a surface irregularity which is evenly distributed over the exposed surface provided that

– at least 50% of the surface of a representative 150mm diameter area lies within a depth of 10mm from a plane taken across the highest points on the exposed surface, and/or

– for surfaces containing cracks, fissures or holes not exceeding 8mm in width nor 10mm in depth, the total area of such cracks, fissures or holes at the surface does not exceed 30% of a representative 150mm diameter area of the exposed surface.

5.1.2 When an exposed surface does not meet the requirements of either 5.1.1a) or 5.1.1b), the product shall, if practicable, be tested in a modified form complying as nearly as possible with the requirements given in 5.1.1. The test report shall state that the product has been tested in a modified form and clearly describe the modification (see clause 13).

### 5.2 Asymmetrical products

A product submitted for this test could have faces which differ or could contain laminations of different materials arranged in a different order in relation to the two faces. If either of the faces can be exposed in use, for example, within a room, cavity or void, then both faces shall be tested.

## 6 Specimen construction and preparation

NOTE – See also A.4.

### 6.1 Specimens

6.1.1 Five specimens shall be tested at each level of irradiance selected and for each different exposed surface.

6.1.2 The specimens shall be representative of the product, square, with sides measuring  $165^{+0}_{-5}$  mm.

6.1.3 Materials and composites of thickness 70mm or less shall be tested using their full thickness.

6.1.4 For materials and composites of thickness greater than 70mm, the requisite specimens shall be obtained by cutting away the unexposed face to reduce the thickness to  $70^{+0}_{-3}$  mm.

6.1.5 When cutting specimens from products with irregular surfaces, the highest point on the surface shall be arranged to occur at the centre of the specimen.

6.1.6 Assemblies shall be tested as specified in 6.1.3 or 6.1.4 as appropriate. However, where thin materials or composites are used in the fabrication of an assembly, the presence of air or an air gap and/or the nature of any underlying construction may significantly affect the ignition characteristics of the

exposed surface. The influence of the underlying layers should be understood and care taken to ensure that the test result obtained on any assembly is relevant to its use in practice (see A.4.1).

When the product is a material or composite which would normally be attached to a well-defined substrate, then it shall be tested in conjunction with that substrate using the recommended fixing technique, e.g. bonded with the appropriate adhesive or mechanically fixed.

Alternatively, where the end-use substrate is non-combustible or of limited combustibility, then the material or composite may be tested using a reference substrate of a density less than the end-use substrate.

See ISO/TR14697 for advice on substrates.

## 6.2 Baseboards

**6.2.1** One baseboard will be required for each test specimen. However, since it will sometimes be possible to re-use the baseboard after test, the total number required will depend on the frequency of testing and the type of product being tested.

**6.2.2** The baseboards shall be square with sides measuring  $165^{+0}_{-5}$  mm and shall be made of non-combustible insulation board of oven dry density  $(825 \pm 125)$  kg/m<sup>3</sup> and nominal thickness 6mm. The thermal inertia of these boards shall be nominally  $9,0 \times 10^4$  W<sup>2</sup>s/m<sup>4</sup>K<sup>2</sup>.

## 6.3 Conditioning of specimens

NOTE — See also A.4.3.

Before test, the specimens and baseboards shall be conditioned to constant mass<sup>1)</sup> at a temperature of  $(23 \pm 2)$ °C and a relative humidity of  $(50 \pm 5)$ % with free access of air to both sides.

## 6.4 Preparation

**6.4.1** A conditioned specimen shall be placed on a baseboard treated according to 6.3 and the combination shall be wrapped in one piece of aluminium foil of nominal thickness 0,02mm from which a circle 140mm diameter has been previously cut (see figure 1). The circular cut-out zone shall be centrally positioned over the upper surface of the specimen. After preparation, the specimen-baseboard combination shall be returned to the conditioning atmosphere until required for test.

**6.4.2** Where a product will normally be backed by air (see 6.1.6), then the specimen shall, where practicable, be backed by an air gap in the test. The air gap shall be formed by including a spacer between the specimen and the baseboard. The spacer shall consist of a piece of non-combustible insulation board of the same size and density as the baseboard, from the centre of which a circular area  $140^{+0}_{-5}$  mm in diameter has been removed. The thickness of the spacer shall correspond to the size of the air gap, if this is known, except that the total thickness of the spacer plus specimen shall not exceed 70mm. If the size of the air gap is not known or the total thickness of the air gap plus specimen exceeds 70mm, then the specimen shall be tested with a spacer which will give a total thickness for the specimen and spacer of  $70^{+0}_{-3}$  mm.

The spacer and baseboard shall be placed for at least 24h in an atmosphere at a temperature of  $(23 \pm 2)$ °C and a relative humidity of  $(50 \pm 5)$ %, with free access of air to both sides of each. The spacer shall

<sup>1</sup> Constant mass is considered to be reached when two successive weighing operations, carried out at an interval of 24h, do not differ by more than 0,1% of the mass of the test piece or 0,1g, whichever is the greater.

then be interposed between the baseboard and the specimen and the combination shall be wrapped in aluminium foil as described in 6.4.1. A clean spacer shall be used for each specimen tested. After preparation the combination shall be returned to the conditioning atmosphere until required for test.

**6.4.3** Baseboards and/or spacers used to back the specimens may be re-used if they are not contaminated. Immediately before re-use, however, they should have been in the conditioning atmosphere specified in 6.3 and 6.4.2 for at least 24h. If there is any doubt about the condition of a baseboard or spacer, it may be placed in a ventilated oven at a temperature of approximately 250°C for a period of 2h in an attempt to remove any volatile residue. If there is still any doubt about the condition, it shall be discarded.

## **6.5 Reflective coatings**

In real fires, metallic coatings which tend to reflect heat may become coated with black soot or tarnish. When assessing the ignitability of materials with a reflective metallic coatings, the product should be assessed both in its virgin state and also with an applied thin coating of matt black water-based emulsion. Apply a coating of carbon black dispersed in organic solvent to give a coverage rate of 5g/m<sup>2</sup> of the carbon black. The coated specimen should then be prepared and tested according to the normal testing procedures in 6.4 and clause 11 respectively.

## **6.6 Dimensionally unstable materials**

This test method may prove unsuitable for materials that change their dimensions substantially when exposed to radiant heat, for example, materials that intumesce or shrink away from the radiator. The irradiance on the surface of such materials may differ significantly from the irradiance set by the temperature controller, either greater or less depending upon the behaviour of the material, which could lead to a worse precision in the repeatability and reproducibility of the method than that indicated in annex D.

## **7 Test apparatus**

All dimensions given in the following description of test apparatus are nominal unless tolerances are specified.

The test apparatus shall consist essentially of a support framework which clamps the test specimen horizontally between a pressing plate and a masking plate such that a defined area of the upper surface of the specimen is exposed to radiation. This radiation shall be provided by a radiator cone positioned above and supported from the specimen support framework. An automated pilot flame application mechanism shall be used to bring a test flame through the radiator cone to a position above the centre of the surface of the specimen. A specimen insertion and location tray shall be used to position the specimen accurately on the pressing plate of the specimen support framework and a screening plate shall be used to shield the surface of the specimen during its insertion into the apparatus.

A general arrangement of a suitable apparatus is shown in figure 2, with detailed drawings in figures 3 to 6.

### **7.1 Specimen support framework, masking plate and pressing plate**

**7.1.1** The specimen support framework and the other parts of the system to hold the specimen in position shall be constructed from stainless steel. It shall consist of a rectangular base-frame made from 25mm x 25mm square tube of 1.5mm wall thickness and shall have overall dimensions of 275mm x 230mm. A horizontal masking plate, 220mm square and 4mm thick, shall be mounted centrally and

260mm above the top of the base-frame on four 16mm diameter legs positioned at the corners of the masking plate. A 150mm diameter circular opening shall be cut centrally in the masking plate, the edges of the hole being chamfered on the top surface of the plate at an angle of 45° and to a horizontal width of 4mm.

**7.1.2** Two vertical guide rods not less than 355mm long of 20mm diameter steel shall be mounted on the base-frame, one at the mid-length of each of the short sides of the frame. A horizontal adjustable bar 25mm x 25mm which can slide on the rods and be locked in position by bolts capable of being tightened by hand shall be mounted below the masking plate and between the vertical guide rods. A vertical central hole and sleeve in the adjustable bar shall be used to locate a sliding vertical rod of 12mm diameter and 148mm long, surmounted by a 180mm square pressing plate 4mm thick. The pressing plate shall be pushed against the underside of the masking plate by the counterweighted pivot arm which shall be mounted below the adjustable horizontal bar and shall press against the bottom of the sliding vertical rod. This can be achieved by an arm about 320mm long.

It shall contain at one end a roller which shall bear against a boss on the bottom of the sliding vertical rod and at the other end an adjustable counterweight.

The counterweight shall be capable of compensating for different masses of specimens and of maintaining a force of approximately 20 N between the upper surface of the specimen and the masking plate. A counterweight of about 3kg has been found to be suitable. An adjustable stop shall be provided to limit upward movement of the pressing plate, due to collapse, softening or melting of the specimen during its exposure, to 5mm. Alternatively spacing blocks between the pressing plate and the masking plate may be used.

**7.1.3** Figure 3 shows details of the specimen support framework.

## **7.2 Radiator cone**

**7.2.1** The radiator cone shall consist of a heating element, of nominal rating 3kW, contained within a stainless steel tube, approximately 3,500mm in length and 8,5mm in diameter, coiled into the shape of a truncated cone and fitted into a shade. The shade shall have an overall height of  $(75 \pm 1)$ mm, an internal diameter of  $(66 \pm 1)$ mm and an internal base diameter of  $(200 \pm 3)$ mm. It shall consist of two layers of 1mm thick stainless steel with a 10mm thickness of ceramic fibre insulation of nominal density 100kg/m<sup>3</sup> sandwiched between them. The heating element shall be fastened to the inside face of the shade by steel pins. At least four clamps shall be used, positioned equidistantly around the perimeter of the shade to prevent additional sagging of the lower coil below the base of the shade. (See figure 4b.)

The upper turn of the heating element shall not obstruct the area of the top aperture of the shade by more than 10% when projected vertically.

**7.2.2** The radiator cone shall be capable of providing irradiance in the range 10 to 70kW/m<sup>2</sup> at the centre of the aperture in the masking plate and in a reference plane coinciding with the underside of the masking plate, when measured as described in 10.2. The distribution of irradiance provided by the cone at the reference plane shall be such that the variation of irradiance within a circle of 50mm diameter, drawn from the centre of the masking plate aperture, shall be not more than  $\pm 3\%$  of that at the centre; the variation of irradiance within a circle of 100mm diameter shall be not more than  $\pm 5\%$  of that at the centre.

The distribution of irradiance shall be determined from readings at the centres of selected 10mm squares forming the grids shown in figure 4d). The tolerances given shall apply to the readings within the grid comprising all the squares shown in figure 4d).

For these measurements, the opening in the masking plate shall be completely filled; it is therefore advisable to employ a number of calibration boards of special horizontal shapes and sizes.

**7.2.3** The radiator cone shall be located and secured from the vertical guide rods of the specimen support framework by clamps which position the lower rim of the radiator cone shade ( $22 \pm 1$ )mm above the upper surface of the masking plate.

**7.2.4** Details of the radiator cone are shown in figure 4b).

**7.2.5** The temperature of the radiator cone shall be controlled by reference to the reading of a thermocouple (primary thermocouple) (7.6) in close and stable thermal contact with the heater element tube. A second thermocouple (secondary thermocouple) shall be attached similarly, mounted in a diametrically opposite position. The thermocouples shall have a speed of response not slower than that of a thermocouple with insulated hot junction in a stainless steel sheath 1mm in diameter. Each thermocouple shall be attached to a coil of the heater element tube which places them between one-third and half way down from the top of the radiator cone. At least 8mm of the end of the thermocouple shall lie in a region of approximately uniform temperature.

A description of methods of attaching thermocouples which have been found satisfactory in practice is given in A.5.1.

### **7.3 Pilot flame application mechanism**

NOTE – See also A.5.2.

**7.3.1** The apparatus shall be provided with a mechanism which is capable of bringing a pilot flame from a re-ignition position outside the radiator cone to the test position within the cone. The mechanism shall be capable of taking the pilot flame through the radiator cone and through the aperture in the masking plate to a maximum distance of 60mm below the underside of the masking plate.

**7.3.2** The pilot flame shall issue from a nozzle made of stainless steel as specified in figure 5, attached near the end of the pilot flame tube.

**7.3.3** The normal position of the pilot flame shall be above the radiator cone and clear of the plume of smoke or decomposition products which may rise through the top of the cone. When in this position the pilot flame nozzle shall be adjacent to a secondary ignition source<sup>2)</sup> having a heat output not greater than 50W which shall be capable of re-igniting the pilot flame should it be extinguished.

**7.3.4** The normal position of the pilot flame shall be such that the flame issues horizontally over the centre point of the aperture in the masking plate and perpendicular to the plane of movement of the pilot arm, with the centre of the orifice in the nozzle positioned ( $10 \pm 1$ )mm above the underside of the masking plate.

**7.3.5** The application mechanism shall automatically bring the pilot flame to the "normal test position" once every  $4^{+0.4}$  s. The pilot flame shall not take longer than 0,5s to travel from the opening at the top of the radiator shade to the test position where it shall remain for  $1^{+0.1}$  s. The time taken for the pilot flame to travel back over the same distance shall not exceed 0,5s.

**7.3.6** The mechanism shall be provided with an adjustable stop which will restrict the lowest point of travel of the pilot flame to any position within the range from 20mm above the test position to 60mm below.

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<sup>2</sup> The secondary ignition source can be a gas flame, hot wire or spark ignited. A propane flame 15mm long, from a nozzle with an internal diameter of 1mm to 2mm, has a heat output of approximately 50W.

**7.3.7** A suitable pilot flame application mechanism is shown in figures 6a), 6b) and 6c).

NOTE — The pilot flame application mechanism should be constructed to a close tolerance since minor changes in the dimensions can lead to changes to the timing as specified in 7.3.5. Small changes can, however, be accommodated by slight changes in the diameter of the slave roller.

#### **7.4 Specimen insertion and location tray**

**7.4.1** The specimen insertion and location tray shall be used to facilitate rapid insertion of the specimen on to the pressing plate and to locate accurately the exposed area of the specimen in relation to the aperture in the masking plate.

**7.4.2** It shall consist essentially of a flat metal plate having lugs on its upper surface to position and hold the specimen. Guides shall be fixed to the lower surface to locate the tray in the apparatus and a stop shall also be provided to bear against the pressing plate, thus limiting the distance of insertion. The tray should be provided with a handle to facilitate use.

**7.4.3** A suitable device is shown in figure 7.

#### **7.5 Specimen screening plate**

**7.5.1** The screening plate shall be designed to slide over the top of the masking plate during the period of insertion of the specimen, thus shielding the specimen from radiation until commencement of the test.

**7.5.2** The plate shall be made from 2mm-thick polished aluminium or stainless steel and shall have overall dimension which allow it to cover the masking plate. It should be provided with a stop, to limit its insertion against the masking plate, and a handle.

**7.5.3** A suitable design is shown in figure 8.

#### **7.6 Temperature controller**

The temperature controller for the radiator cone shall be of the proportional integral and derivative type ("3-term" controller) with thyristor stack fast-cycle or phase angle (see A.5.3) control of not less than 15A maximum rating. Capacity for adjustment of integral times between about 10s and 150s, and differential times between about 2s and 30s, shall be provided to permit reasonable matching with the response characteristics of the heater. The temperature at which the heater is to be controlled shall be set on a scale capable of being read to  $\pm 2^{\circ}\text{C}$ . An input range of temperature of about  $0^{\circ}\text{C}$  to  $1000^{\circ}\text{C}$  is suitable. (An irradiance of  $50\text{kW}/\text{m}^2$  will be given by a heater temperature in the region of  $800^{\circ}\text{C}$ .) Automatic cold junction compensation for the thermocouple shall be provided.

Desirable features are a meter to indicate the output to the heater and a control which, in the event of an open circuit in the thermocouple line, will cause the temperature to fall to near the bottom of its range.

The monitor heater temperature, particularly to show the operator when the heater has attained temperature equilibrium, heater temperature shall be indicated by a meter capable of being read to  $\pm 2^{\circ}\text{C}$ . This may be incorporated in the controller or separate.

#### **7.7 Radiometer (heat flux meter)**

The radiometer shall be of the Schmidt Boelter or Gardon type with a range of 0 to  $70\text{kW}/\text{m}^2$ . The target receiving radiation, and possibly to a small extent convection, shall be flat, circular, not more than 10mm in diameter and coated with a durable matt black finish. The target shall be contained within a water-



cooled body the front face of which shall be of highly polished metal, flat, coinciding with the plane of the target and circular, with a diameter of about 25mm.

Radiation shall not pass through any window before reaching the target. The instrument shall be robust, simple to set up and use, insensitive to draughts, and stable in calibration. The instrument shall have an accuracy of within  $\pm 3\%$  and a repeatability within 0,5%.

The calibration of the radiometer shall be checked whenever a recalibration of the apparatus is carried out (see 10.2), by comparison with an instrument held as a reference standard and not used for any other purpose. The reference standard instrument shall be fully calibrated at yearly intervals.

#### **7.8 Millivolt measuring device**

This shall be compatible with the output from the radiometer specified in 7.7. It shall have a full scale deflection, sensitivity and accuracy which enables the irradiance measure by the radiometer to be resolved to 0,5kW/m<sup>2</sup>.

#### **7.9 Secondary thermocouple monitoring device**

To monitor the secondary thermocouple, an instrument is required with a resolution equivalent to  $\pm 2^\circ\text{C}$ . This may read directly in temperature or in millivolts. Allowance or automatic compensation for cold junction temperature shall be made. If a separate device is used to monitor heater temperature, this may, with a suitable switch connection, also be used to monitor the secondary thermocouple.

#### **7.10 Timing device (timer)**

This shall be capable of recording elapsed time to the nearest second and shall be accurate to within 1s in 1h.

#### **7.11 Air and propane supplies**

Air and propane shall be fed to the pilot flame (see 7.3) via regulating valves, filters (if necessary), flow meters, non-return valves, a suitable junction connection and a flame arrester as shown in figure 10.

##### **7.11.1 Gas regulating valves**

These shall be capable of adjusting the pressure and flow of propane and air to the pilot flame to the levels required by 9.2.

##### **7.11.2 Filters**

Filters may need to be installed in the propane and/or air lines to avoid the readings of the flow-meters being affected by impurities (for example oil droplets) carried in the flow.

##### **7.11.3 Flow-meters**

These shall be capable of measuring the flow-rates of propane and air to the pilot flame to an accuracy of at least 5%.

##### **7.11.4 Non-return valves**

A suitable non-return valve shall be included in both air and propane lines, sited as close to the junction point as possible.

#### **7.11.5 Flame arrester**

A flame arrester (see figure 6a) shall be mounted at the point of entry of the propane air mixture to the pilot flame arm.

#### **7.11.6 Connections**

All connections with flexible tubing shall be firmly attached with suitable clips.

#### **7.12 Calibration board**

The board shall be made of ceramic fibre of density  $(200 \pm 50)\text{kg/m}^3$ , and shall be square, with sides measuring  $165_{-5}^0$  mm and of thickness not less than  $20_{-0}^{+5}$  mm.

A suitable hole or groove cut to fit closely around the radiometer shall be cut in the centre of the board. The target of the radiometer shall be in the plane of the upper surface of the board. If additional support for the radiometer is required, it shall be provided from below the calibration board.

#### **7.13 Dummy specimen board**

The dummy specimen board shall be constructed as specified in figure 11. The necessary total thickness of ceramic fibre board may be built up from a number of thinner sheets attached to each other by adhesive or long fine pins.

#### **7.14 Extinguishing board**

The extinguishing board shall be made of the same material as the baseboards (6.2) and shall have nominal dimensions of 300mm x 185mm x 6mm.

#### **7.15 Oven**

If it is necessary to meet the recommendation given in 6.4.3, then a ventilated oven capable of maintaining a temperature of approximately 250°C is required.

#### **7.16 Specimen conditioning cabinet**

The specimen conditioning cabinet shall be capable of maintaining a constant temperature of  $(23 \pm 2)^\circ\text{C}$  and a relative humidity of  $(50 \pm 5)\%$ .

#### **7.17 Balance**

The balance shall have a nominal capacity of 5kg and shall be capable of being read to the nearest 0,1g.

### **8 Test environment**

**8.1** The test shall be carried out in an environment essentially free of air currents and protected, where necessary, by a screen. The air velocity close to the test apparatus should be not more than 0,2m/s. The operator should be protected from any products of combustion generated by the specimen. The effluent gases shall be extracted without causing forced ventilation over the apparatus.

**8.2** A suitable design for screening the apparatus from draughts and exhausting the effluent gases is shown in figure 9.

## **9 Setting-up procedure and requirements**

### **9.1 Siting the apparatus**

The apparatus shall be placed in an environment essentially free of air currents (see clause 8).

### **9.2 Pilot flame**

NOTE— See also A.5.2.

The pilot flame nozzle (see 7.3) shall be fed with a mixture of propane and air which is achieved by regulating the propane flow-rate to 19 to 20ml/min and the air flow-rate to 160 to 180ml/min. These flow-rates shall be measured after the pressure and flow regulating valves and shall be fed directly to the pilot flame from the flow meters so that the pressure is nominally atmospheric.

### **9.3 Electrical requirements**

**9.3.1** The heating element of the radiometer cone (7.2) shall be connected to the output from the thyristor of the temperature controller as shown in figure 10. No element or wiring in this circuit shall be changed between calibration and testing. The primary thermocouple shall be connected to the temperature controller and its temperature-monitoring device. The secondary thermocouple shall be connected to its monitoring device (7.9).

**9.3.2** The framework of the apparatus shall be provided with a good electrical earth.

### **9.4 Precautions against electrical interference**

The radiometer shall be connected to the millivolt measuring device (7.8) using leads which should be screened to minimize any electrical interference to the signal. The radiometer shall be earthed back to the millivolt measuring device and by no other route (i.e. not to the earthed frame of the apparatus). All connections shall be thoroughly checked to ensure good electrical contact.

## **10 Calibration**

### **10.1 Installation of radiometer**

For calibration of the apparatus, the radiometer (7.7) shall be installed in the hole or groove of the calibration board (7.12).

### **10.2 Calibration procedure**

Calibration procedure shall be as follows.

- a) Set up the apparatus as described in clause 9, except that the pilot flame mechanism shall be kept in the re-ignition position with the gas supply turned off throughout the calibration procedure.
- b) Place the calibration board (7.12) in the apparatus in the specimen position so that the target of the radiometer (7.7) is located centrally within the circular opening of the masking plate, in the plane of the bottom face of the masking plate.

c) Switch on the electricity supply and establish the temperature settings of the controller required to produce irradiances at the centre of the circular opening in the masking plate of 10, 20, 30, 40, 50, 60 and 70kW/m<sup>2</sup>. Adjustments near the final setting for the heater temperature should be followed by a 5-min period without further adjustment to ensure that the remainder of the apparatus has attained sufficient temperature equilibrium.

At each full equilibrium, read and record the secondary thermocouple monitor. These readings are to enable a close and independent check to be made on the temperature of the heater during testing.

d) Carry out this procedure at least twice, the first time at setting of increasing temperature and the second time at decreasing settings.

The values should be repeatable to within  $\pm 5^{\circ}\text{C}$ . Repeatability values outside these limits indicate possible defects in control of monitoring equipment, or significant changes in the test environment, which shall be corrected before any further calibrations are carried out.

### 10.3 Calibration check

The irradiance produced by the temperature setting which the initial calibration has shown to correspond to an irradiance of 30kW/m<sup>2</sup> shall be frequently checked (at least once every 50 operating hours) and the apparatus shall be recalibrated if such a check reveals a deviation greater than 0,6kW/m<sup>2</sup>.

## 11 Test procedure

### 11.1 Initial procedure

The initial procedure shall be as follows.

- a) Set up the apparatus as described in clause 9.
- b) Weigh a prepared specimen-baseboard combination (6.4.1) and return to the conditioning atmosphere.
- c) Adjust the counterweight mechanism to give a force of  $(20 \pm 2)\text{N}$  between the upper surface of the specimen and the underside of the masking plate (see 7.1.2, A.6.1 and A.6.2), when the specimen-baseboard combination is positioned on the pressing plate in the insertion and location tray. This adjustment may be made by methods indicated in A.6.1 but using a dummy of the same mass as the specimen-baseboard combination instead of a prepared and conditioned specimen.
- d) Insert the dummy specimen-board (7.13).
- e) Adjust the temperature setting of the controller to the appropriate value established by the calibration procedure to correspond to 50kW/m<sup>2</sup> (or other levels as required).
- f) Allow the apparatus to heat up to equilibrium. When the heater has attained temperature equilibrium, as shown by the indicating meter of the temperature controller, a further 5 min should be allowed to elapse before commencing exposure of a specimen.
- g) Check that the reading of the secondary thermocouple is within the equivalent of  $\pm 2^{\circ}\text{C}$  of the value established during the calibration procedure (10.2). A deviation outside this tolerance indicates the need for a complete re-calibration.

- h) Remove a prepared specimen from the conditioning cabinet (7.16) and place it on the insertion and location tray (7.4).
- i) Place the specimen screening plate on top of the masking plate.
- j) Start the pilot flame application mechanism (7.3).
- k) Use the adjustable stop on the pilot flame mechanism to ensure a distance of 10mm is maintained between the surface of the dummy specimen board and the pilot flame.
- l) Place the specimen screening plate on top of the masking plate
- m) Lower the pressing plate, remove the dummy specimen board and replace it with the insertion and location tray containing the specimen.
- n) Release the pressing plate.
- p) When the pilot flame is at the re-ignition position, simultaneously remove the specimen screening plate and start the timer (7.10).

## 11.2 Time permitted for test initiation

All operations detailed in 11.1 i) to m) shall be completed within 15s.

## 11.3 Conduct and termination of test

**11.3.1** If sustained surface ignition of the specimen occurs (see 3.9), the timer shall be stopped. Any flames shall immediately be extinguished by placing the extinguishing board (7.14) on top of the masking plate and the pilot flame application mechanism shall be stopped. The tray and remains of the specimen shall then be quickly removed and replaced by the dummy specimen board. The extinguishing board shall then be removed as quickly as possible (see A.6.3).

**11.3.2** If no sustained surface ignition of the specimen occurs within 15min, the test shall be stopped by placing the extinguishing board on top of the masking plate and the pilot flame application mechanism shall be stopped. The specimen shall then be removed and replaced by the dummy specimen board. The extinguishing board shall then be removed as quickly as possible.

**11.3.3** Continue the test until termination even if transitory surface ignitions and/or plume ignitions occur which should be noted (see 11.5.2).

## 11.4 Repeat tests

**11.4.1** Operations 11.1 h) to p) and 11.3 shall be repeated with four more specimens at the same irradiance after allowing sufficient time between applications to allow the apparatus to reach thermal equilibrium (see A.6.3).

**11.4.2** If sustained surface ignition occurs with any specimen in a set of five at a given irradiance, a further set of five specimens shall be tested at the next lower level of irradiance (or at any other set lower level).

**11.4.3** Operation 11.4.2 shall be repeated as necessary until a set of five specimens has been tested at each required irradiance.

**11.4.4** If no sustained surface ignition occurs (see 11.3.2) with all specimens in a set of five at a given irradiance, a further set of five specimens shall be tested at the next highest level of irradiance (or at any other set higher level).

**11.4.5** When adjusting the heater to the next level of irradiance, sufficient time shall be allowed for the apparatus to reach thermal equilibrium following the change in temperature setting (see A.6.3).

At full equilibrium the reading of the secondary thermocouple should be within  $\pm 2^{\circ}\text{C}$  of the value established during the calibration procedure (10.2).

## **11.5 Observations during test**

**11.5.1** For each specimen tested, the time at which sustained surface ignition occurs shall be noted (see 3.9).

**11.5.2** Observations shall be made during each test of the general behaviour of the specimen and, in particular, note should be made of the following:

- a) the time, position and nature of other ignitions;
- b) glowing decomposition of the specimen;
- c) melting, foaming, spalling, cracking, expansion or shrinkage of the exposed surface of the specimen.

## **11.6 Special procedures**

### **11.6.1 Soft and softening products**

**11.6.1.1** For some soft products, especially low-density products such as glass- or mineral-fibre products with or without coatings, the pressure of the pressing plate may cause some compression of the edges of the specimen so that the exposed face of the specimen is not flat but convex upwards. This can occur even without heating from the radiator cone.

In order that the specimen should not be subjected to an irradiance higher than that for a flat, stable specimen, an adjustable stop should be installed and operated on the pressing plate mechanism to avoid the crushing of the aluminium foil wrapping, to maintain the surface of the specimen flat and to preserve the nominal thickness of the product. Alternatively, spacing blocks between the pressing plate and the masking plate may be used.

**11.6.1.2** For specimens which are likely to contract, soften or melt away when heated it is necessary to prevent the pressing plate (7.1.2) from unduly crushing the aluminium foil wrapping on the edge of the specimen. This can be accomplished by an adjustable stop on the pressing plate mechanism or spacing blocks between the pressing plate and the masking plate.

**11.6.1.3** With certain products the pilot flame application mechanism may not act satisfactorily. For example, some materials become sticky when heated and can be drawn up in threads, some materials are or become soft enough for the pilot flame arm to bury itself, some materials intumesce and produce a foamed char "crust" having little mechanical strength. With these products it will be necessary to operate the adjustable stop on the travel of the pilot flame application mechanism to bring it close to, but not touching, the exposed surface of the specimen (see A.6.4).

**11.6.1.4** Certain materials (e.g. PVC) may contain high concentrations of flame retardants. With these products, the copious fumes generated on irradiating can extinguish the pilot flame and prevent its re-ignition by the secondary ignition source. If this situation occurs repeatedly within 15 min, when

reasonable attempts to re-light the pilot flame have been made, the results should be given as "no sustained surface ignition under these test conditions: pilot flame repeatedly extinguished by decomposition products".

#### **11.6.2 Products with reflective coatings**

For products with reflective coatings, whether the matt black coating has been applied or not, the pilot flame application mechanism may not be satisfactory since the mechanism may damage the surface coating or reflective film. With these products, the adjustable stop on the travel of the pilot flame application mechanism should be used to bring the flame close to but not touching the exposed surface of the specimen (see A.6.4).

#### **11.6.3 Assemblies containing an air gap**

When an assembly is to be used with an air gap behind the exposed surface, care shall be taken to ensure that the pilot flame nozzle cannot penetrate the surface of the specimen and enter the void behind it. If necessary the adjustable stop shall be operated to prevent this from occurring.

#### **11.6.4 Products with irregular surfaces**

When testing a product with an irregular surface (complying with 5.1.1.b), it may be necessary to operate the adjustable stop on the travel of the pilot flame application mechanism, to ensure that, initially, the flame issues from the nozzle orifice at a distance of 10mm above the highest point of the specimen. If necessary, the adjustable stop should be operated to follow any change in surface shape.

### **12 Expression of results**

**12.1** At each irradiance, the time to sustained surface ignition, in seconds, shall be reported for each of the five specimens tested.

**12.2** If for any specimen no sustained surface ignition occurs within 15 min (see 11.3.2), the result for that specimen at that irradiance shall be given as "no sustained surface ignition".

**12.3** If no sustained surface ignition occurs with all specimens in a set of five at a given irradiance, then tests at lower irradiances need not be carried out, but shall be reported as "not necessary due to non-ignition at higher irradiances".

### **13 Test report**

The test report shall be as comprehensive as possible and shall quote the individual specimen ignition times for each irradiance tested. Any observations made during the test and comments on any difficulties experienced during testing shall also be given. The following essential information shall also be given in the test report and shall additionally be included in a summary test report:

- a) name and address of test laboratory;
- b) name and address of sponsor;
- c) name and address of manufacturer/supplier;

- d) full description of the product tested including tradename, together with its composition, construction, orientation, thickness, density and mass of the conditioned specimen before test and where appropriate the face subjected to test (note particularly 5.1.2); details of substrates used and fixing methods shall be given; with composites and assemblies the thickness and density of each of the components shall be given, together with the apparent (i.e. overall) density of the whole; details of any surface treatment (e.g. black coating etc.) shall also be included;
- e) for some products the date of manufacture and information about subsequent treatment and/or exposure may be of importance;
- f) the statement: "The test results relate only to the behaviour of the test specimens of a product under the particular conditions of the test; they are not intended to be the sole criterion for assessing the potential fire hazard of the products in use".

Dimensions in millimetres

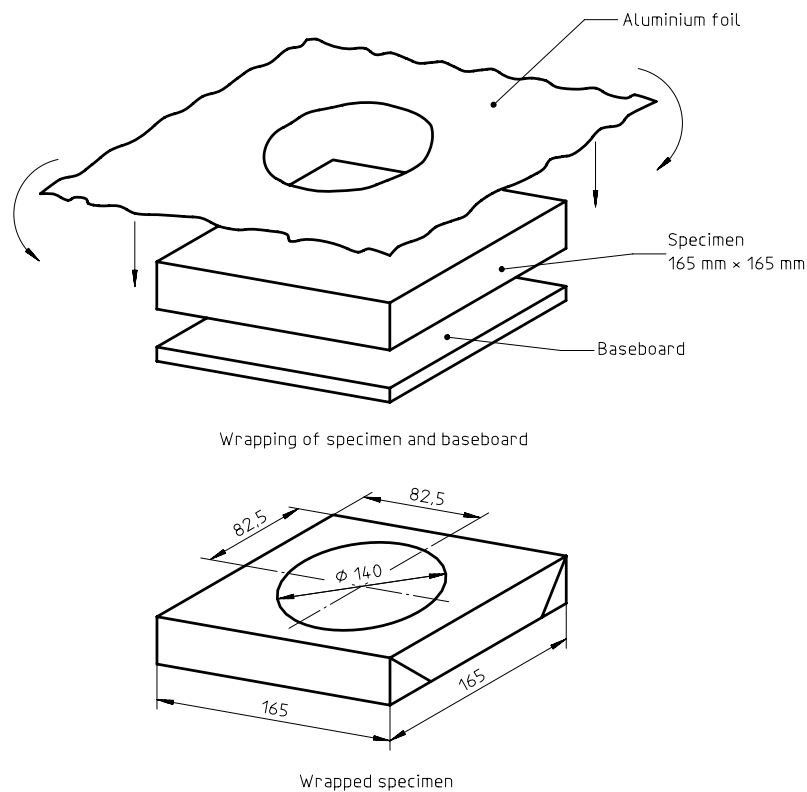


Figure 1 — Wrapping of the specimen



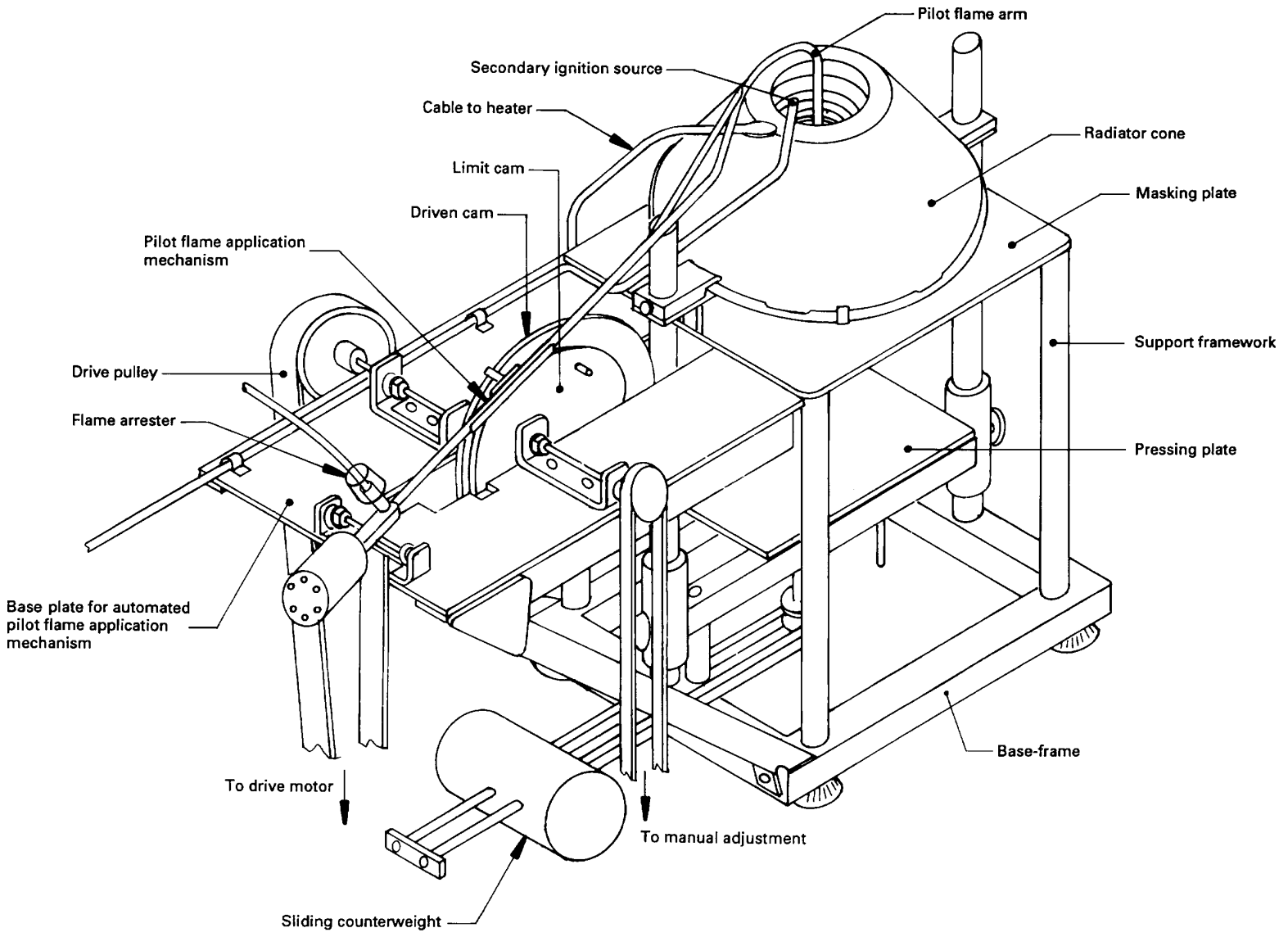


Figure 2 — Ignitability test apparatus — General view

Dimensions in millimetres

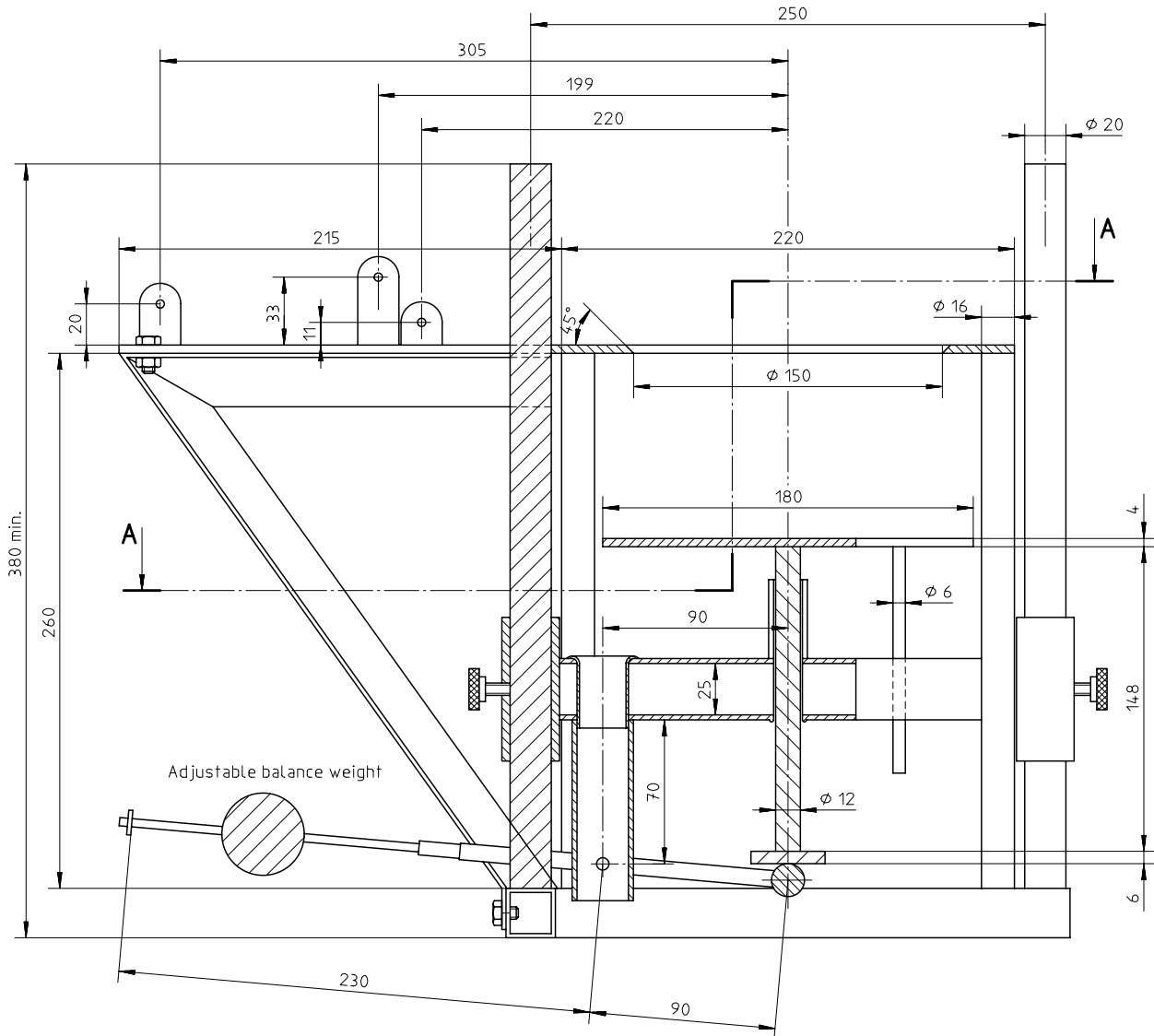


Figure 3a) — Specimen support framework — Part sectional elevation along B-B [figure 3b)]

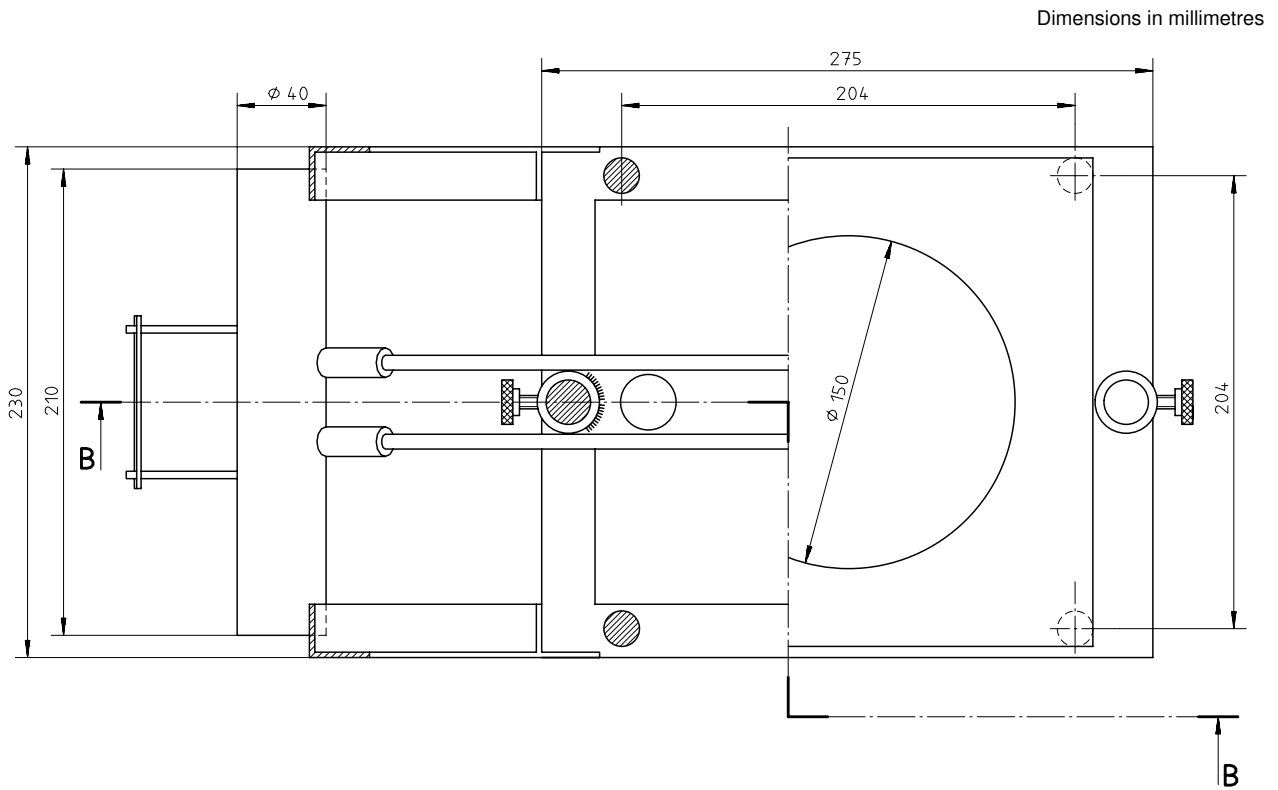


Figure 3b) — Specimen support framework — Part sectional plan along A-A [figure 3a)]

Dimensions in millimetres

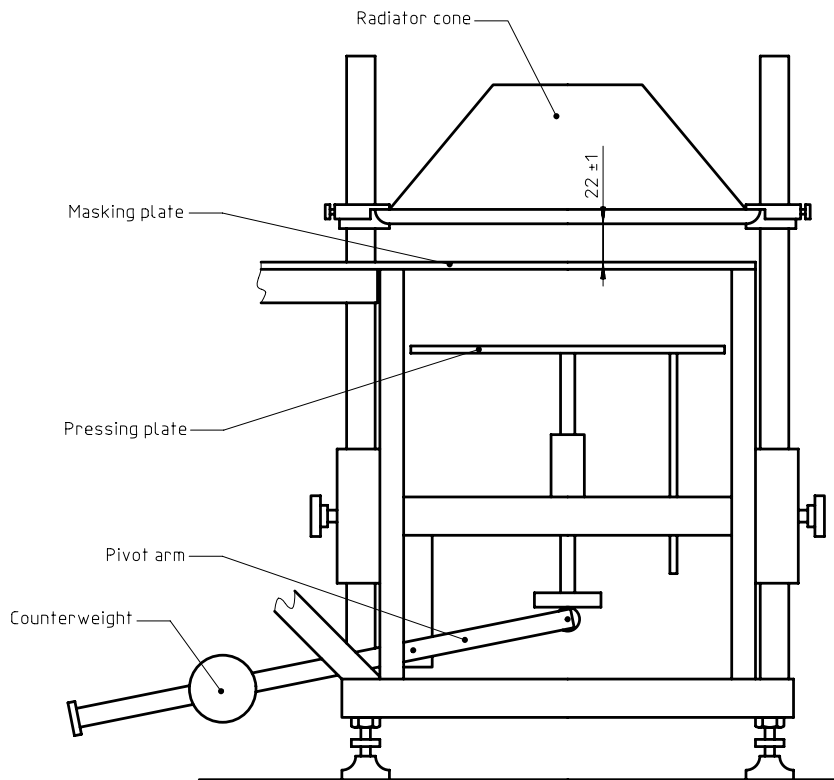


Figure 4a) — Specimen support framework and radiator cone

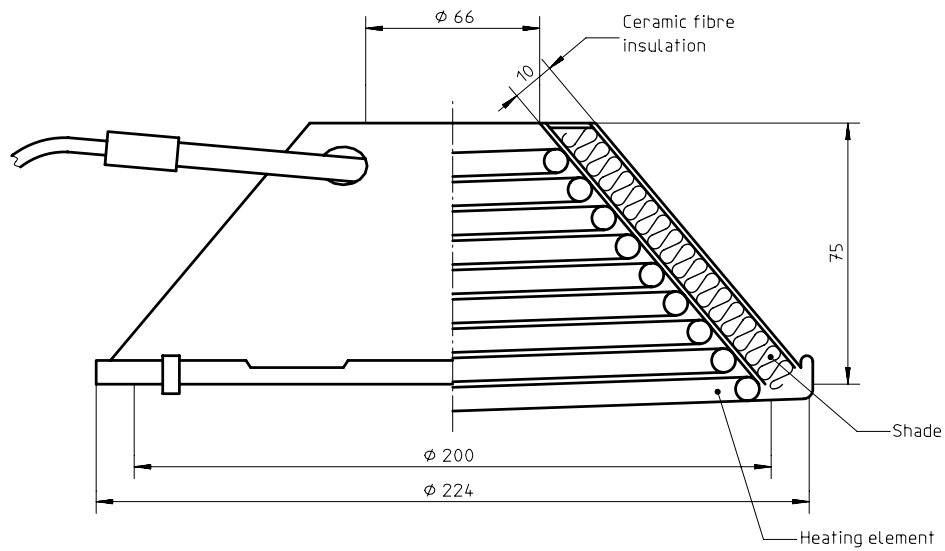
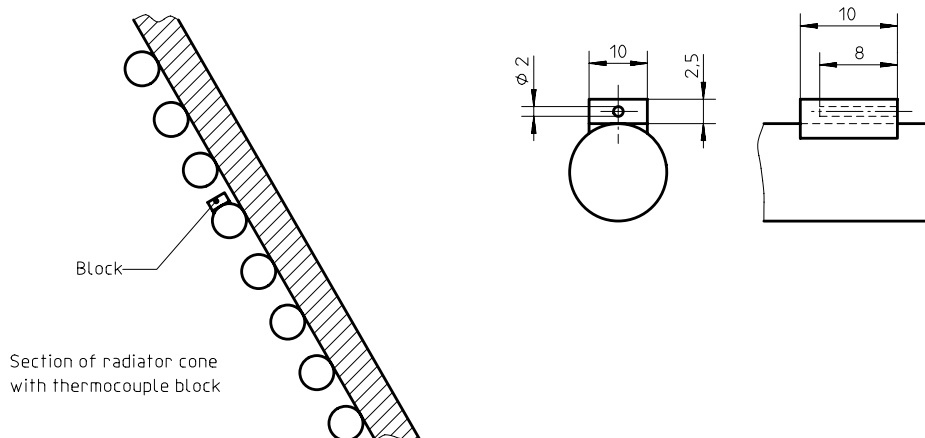


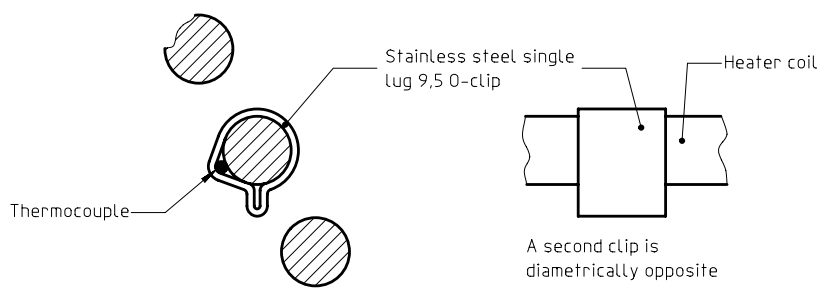
Figure 4b) — Radiator cone

Dimensions in millimetres

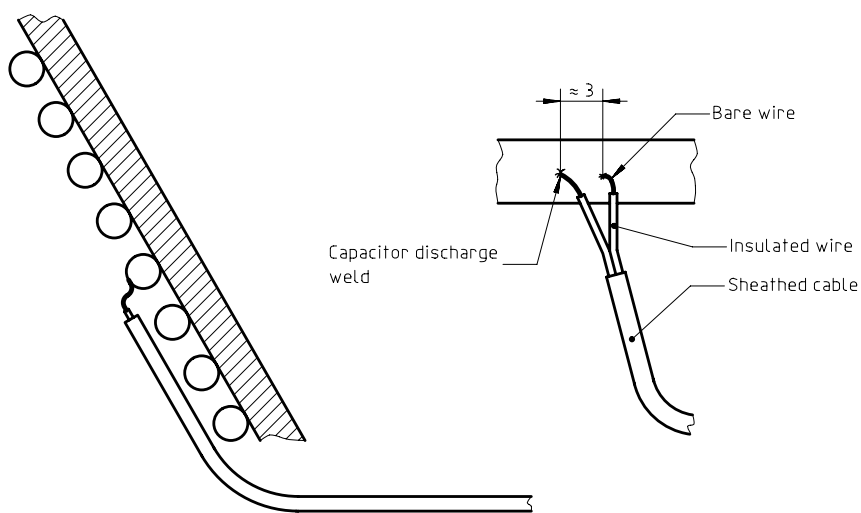


NOTE - A second block is diametrically opposite.

**Block method**

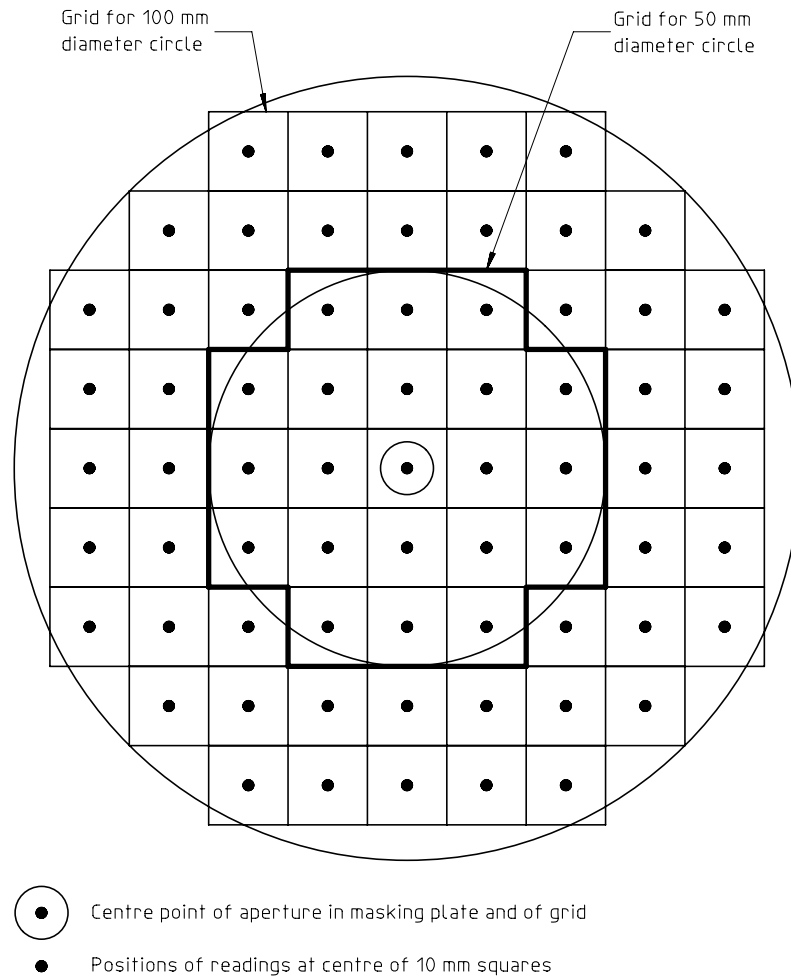


**Clamp method**



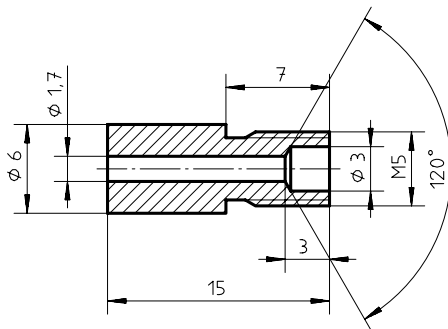
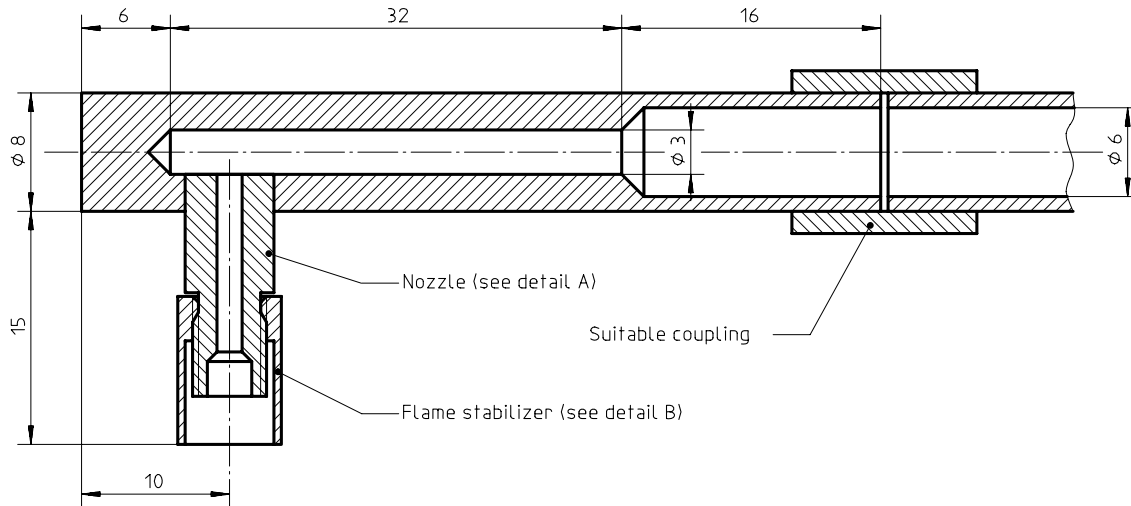
**Welding method**

**Figure 4c) — Methods for attachment of thermocouples to heater coil**

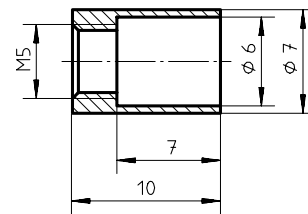


**Figure 4d) — Grids of readings for irradiance distribution**

Dimensions in millimetres



Detail A - Nozzle



Detail B - Flame stabilizer

**Figure 5 — Pilot flame nozzle**

Dimensions in millimetres

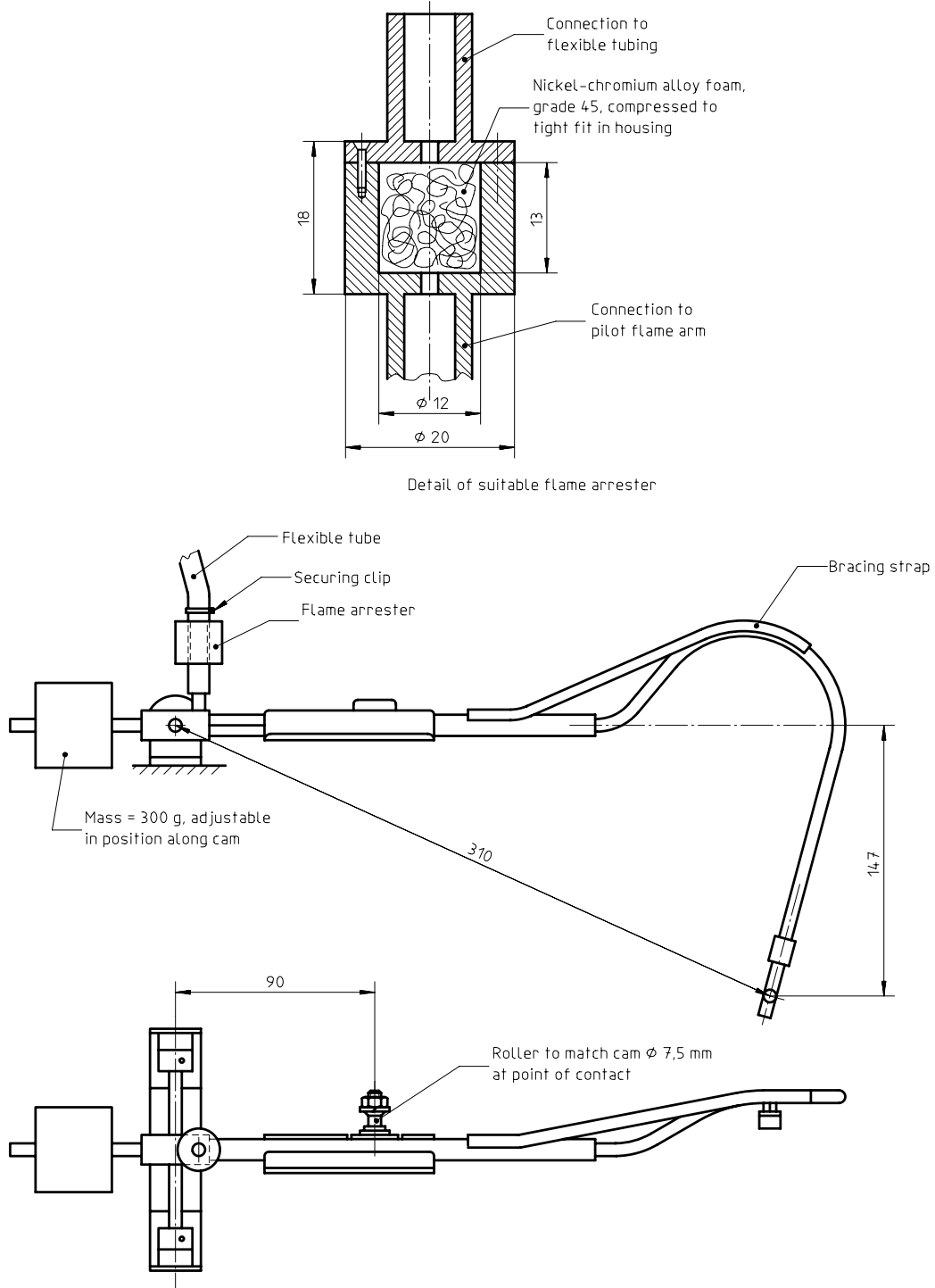


Figure 6a) — Pilot flame application mechanism — Pilot flame arm



Dimensions in millimetres

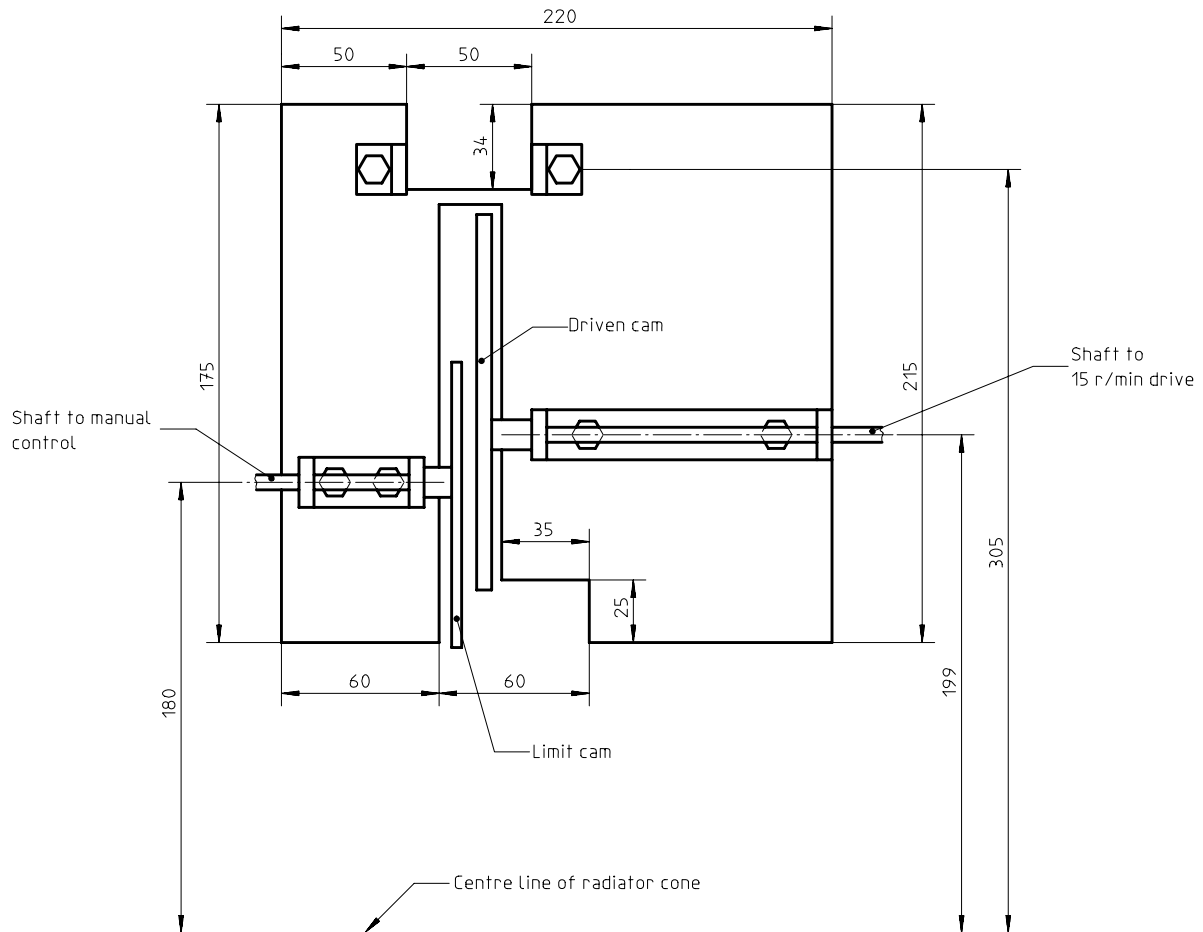


Figure 6b) — Pilot flame application mechanism — Base plate (plan view)

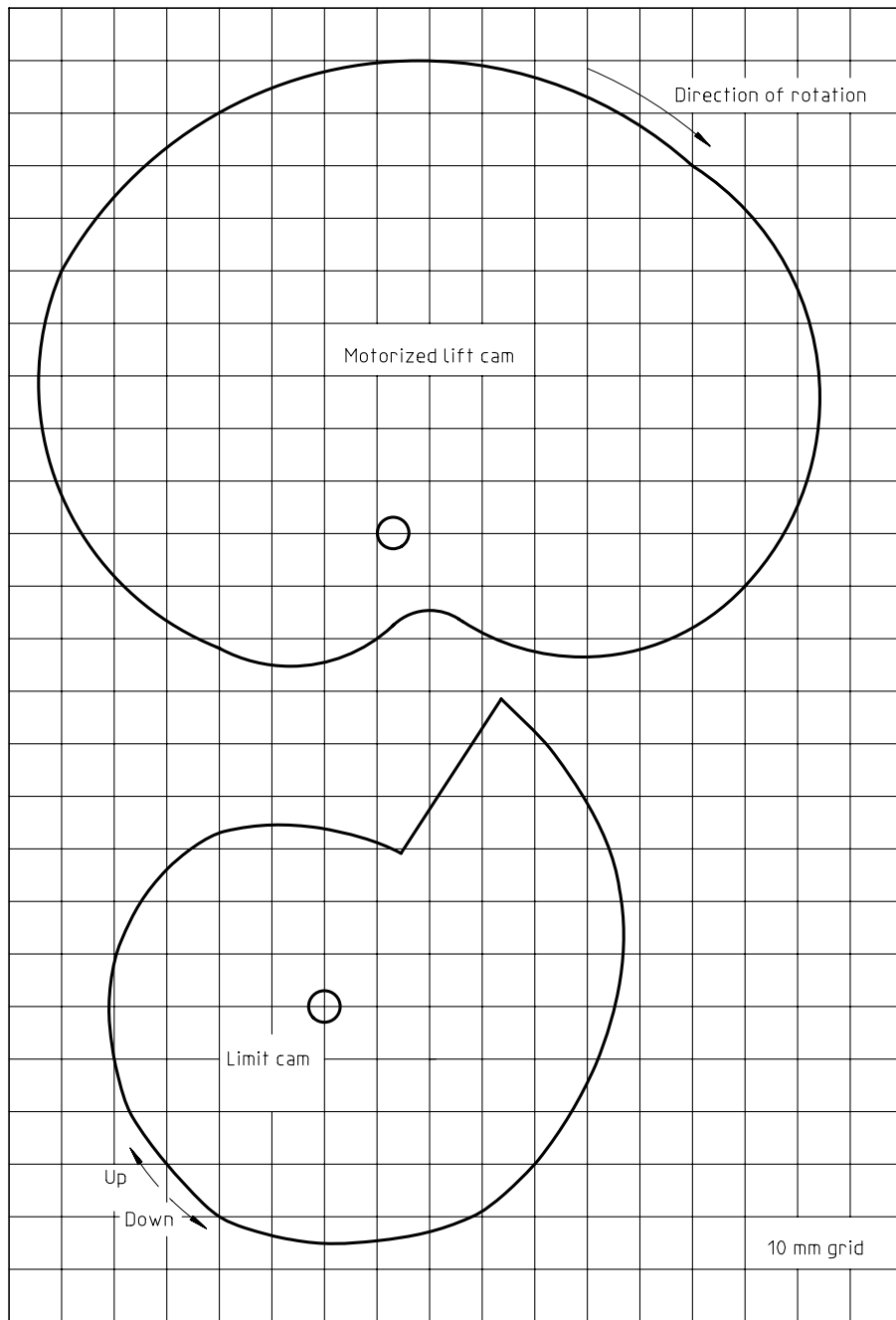
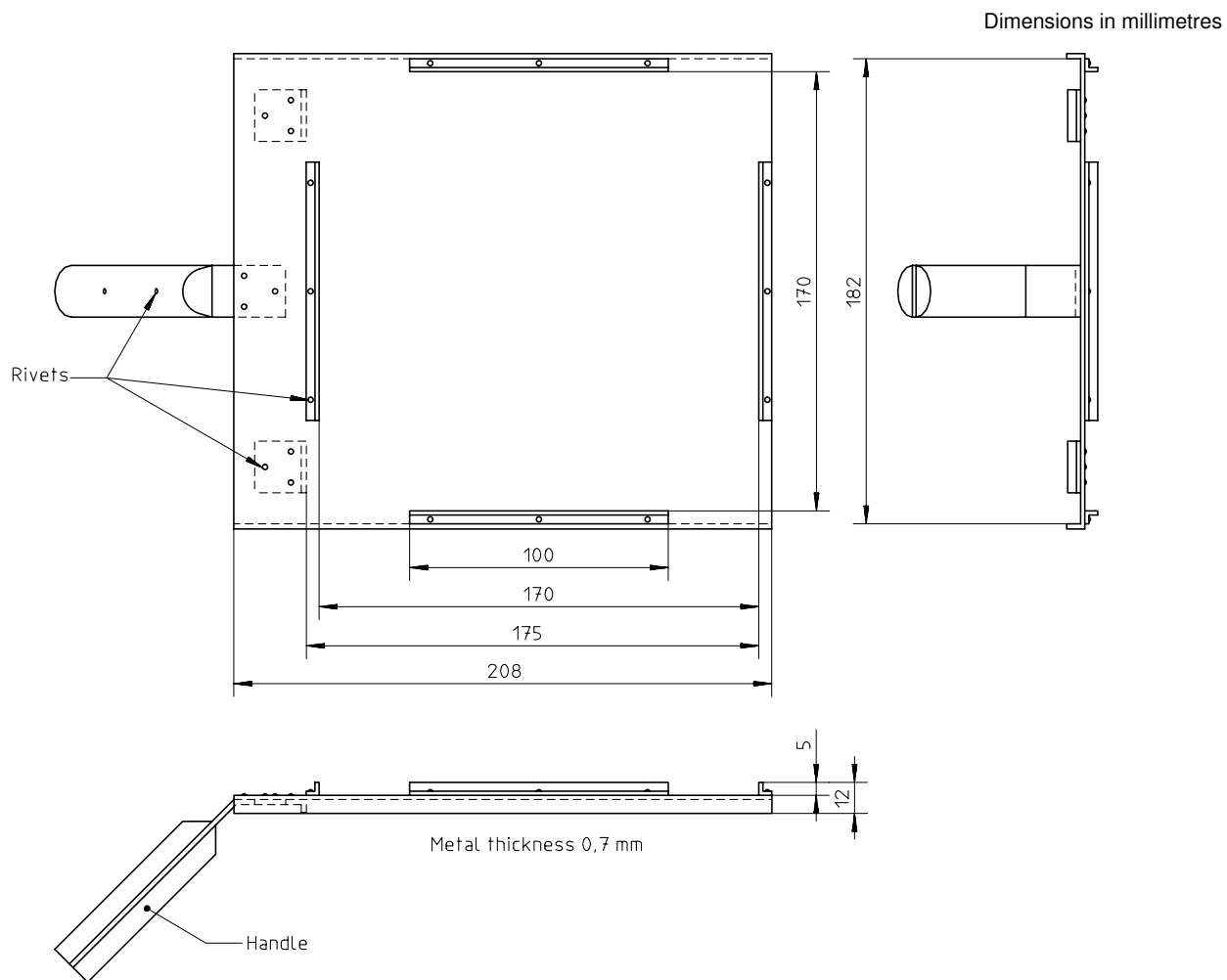
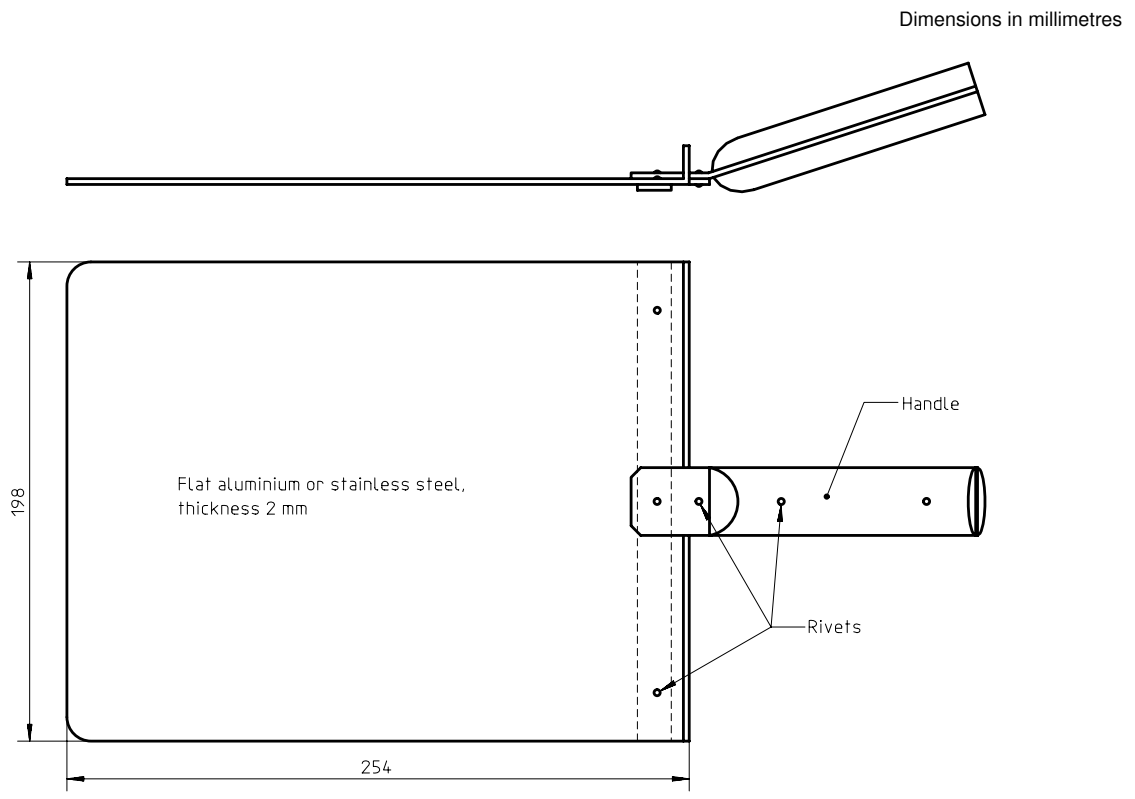


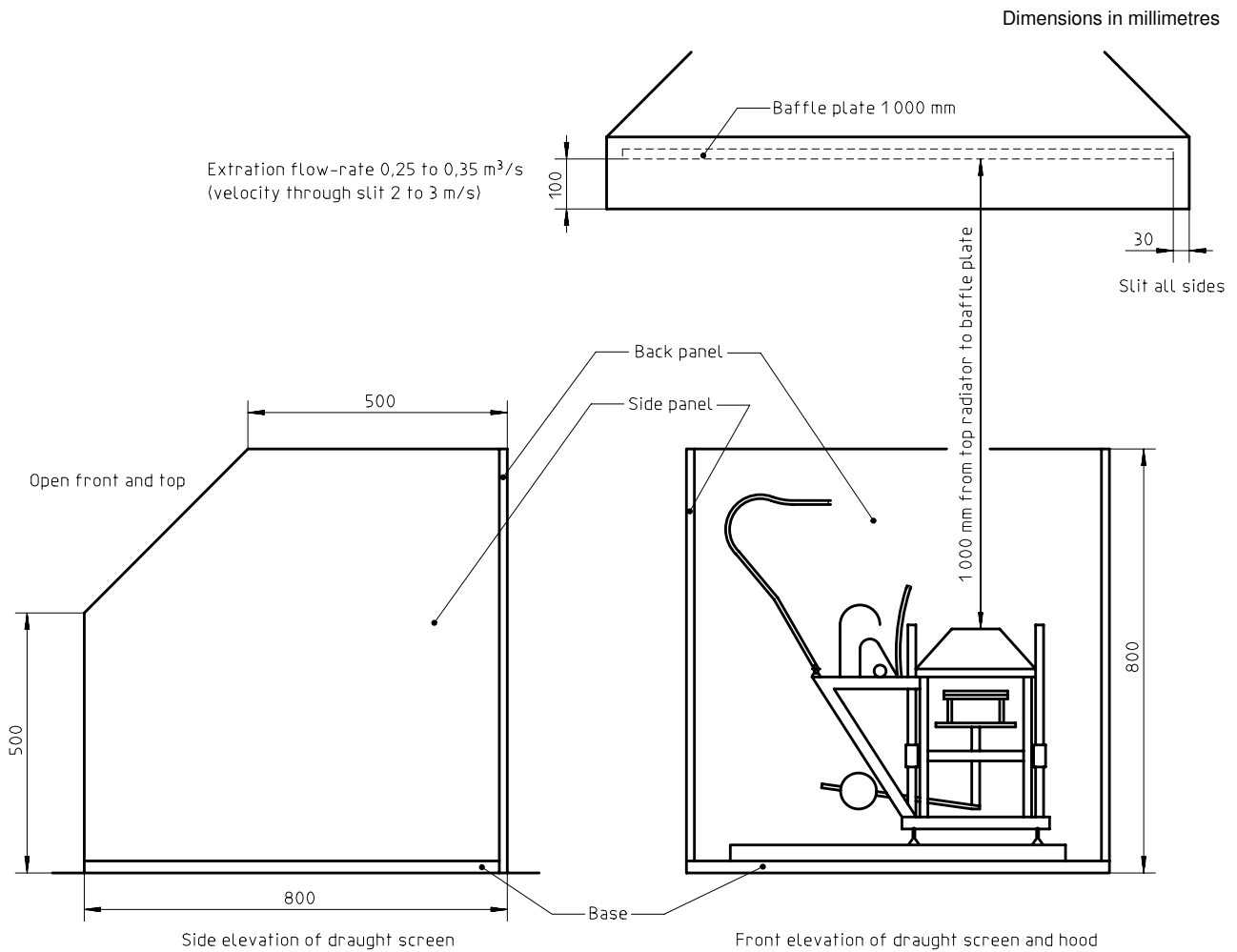
Figure 6c) — Pilot flame application mechanism — Cam geometry



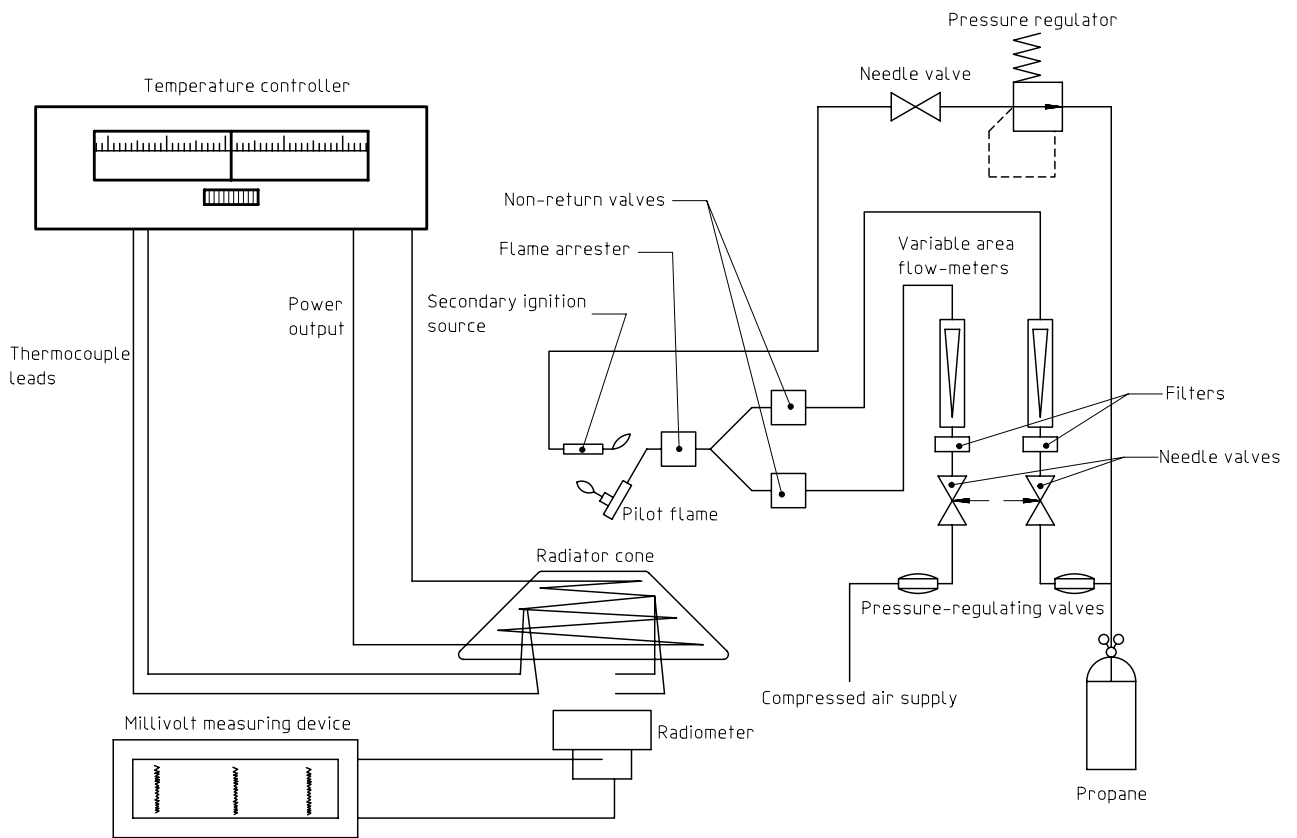
**Figure 7 — Specimen insertion and location tray**



**Figure 8 — Specimen screening plate**



**Figure 9 — Extraction hood and draught screen for ignitability apparatus**



**Figure 10 — Diagrammatic arrangement of apparatus and additional equipment**

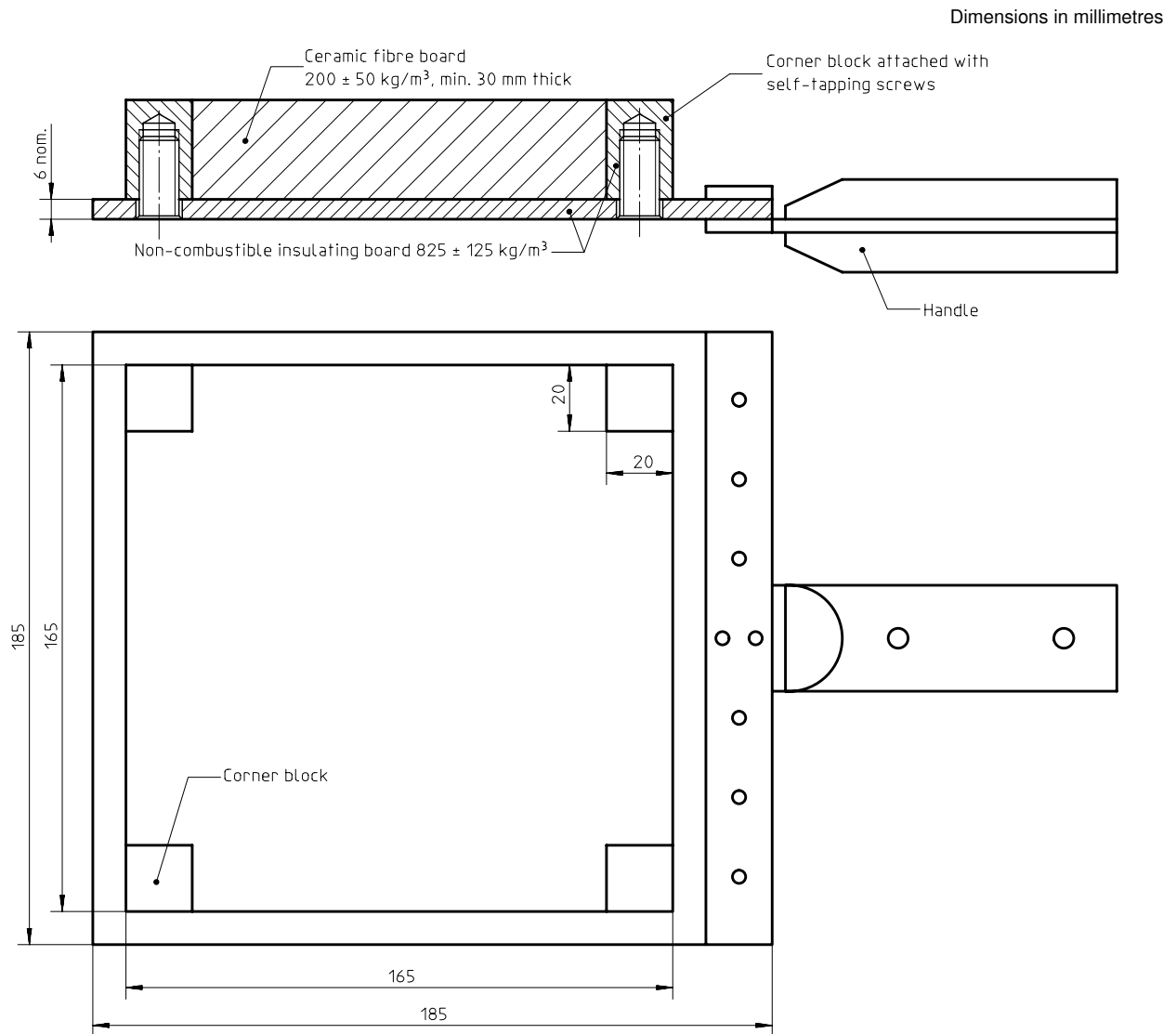


Figure 11 — Dummy specimen board

## **Annex A** (informative)

### **Commentary on the text and guidance notes for operators**

#### **Introduction**

This annex aims to provide the test operator, and perhaps the user of the test result, with background information and more explicit details of some of the requirements and procedures given in this specification.

#### **A.1 Definitions**

For the purpose of clarity, the material which is the subject of investigation has been defined as a product, and this can be a single material, a composite or an assembly.

It is known that the ignition characteristics of a material may vary considerably when used in different conditions, for example, a thick material backed with a lightweight insulating substrate will behave differently when backed by a dense high-conductivity material. It is important that consideration is given to the actual usage of the material in practice.

The definition of the three types of product allows clarification in the test report of the way in which a test was conducted on a building product

#### **A.2 Principles of the test**

This test method examines the ability of a material, when the surface is exposed to radiant heat, to produce volatile gases which would sustained ignition in the presence of a small ignition source. It does not study the ability of the material to resist ignition when subjected to direct flame impingement in the absence of additional impressed radiation, which will depend upon the application time of the igniting flame and the total energy release in the ignition flame.

It has been shown (see reference [4]) that before ignition substantial absorption of radiation can take place in the plume of decomposition products rising from a specimen exposed in this apparatus.

#### **A.3 Suitability of a product for testing**

**A.3.1** The test method and equipment, although designed to examine flat surfaces, can accept a limited amount of surface irregularity. Surface characteristics of certain building products have been identified and have been considered in two groups, i.e. regularly formed or grooved surfaces (for example corrugated sheets) and embossed, scarred or punctured surfaces (for example patterned mineral fibre tiles). Limiting dimensions have been chosen to ensure that an irregular surface is subjected to the same irradiance as a flat surface and that the majority of the irregular surface is at the test plane.

**A.3.2** The test specimens shall be representative of the surface of the material to be tested. If a representative area cannot be obtained, it may be necessary to conduct more than one test for a full evaluation of the variation in the product's surface. Simulation of a product surface, which does not satisfy the dimensional limits, in modified flat form may also require more than one test for a full



evaluation of the variation in the product's surface. In either case the test results shall be separately recorded.

**A.3.3** When an assessment of the area of surface irregularity is required, this can be carried out by machining the surface to a depth of 10mm below the highest point and estimating the machined surface area.

**A.3.4** The results of the test with products of low absorptance (for example shiny metallic surfaces, glossy enamelled surfaces) need to be treated with caution (see annex C). The additional test on a product with a blackened surface may provide some indication of the range of ignitability performances which may be seen in a fire.

**A.3.5** It has to be realised that for large initial thicknesses of those kinds of materials which melt away on heating, the test is to some extent unsuitable since the irradiance at the melted material (on top of the baseboard) will be lower than at the original surface of the material, and the dwell time of the pilot flame close to the melted material will be reduced.

**A.3.6** The test cannot be expected to yield a meaningful result with products which intumesce considerably, although some intumescence can be accommodated (nearly up to the plane of the bottom of the shade) if necessary with suitable manual adjustment of the diving pilot flame (11.6.1.3).

#### **A.4 Specimen construction and preparation**

**A.4.1** Careful consideration should be given to the mounting of specimens to ensure that they represent the building product in practice.

With thin materials or composites, particularly those with a high thermal conductivity, the presence of an air gap and the nature of any underlying construction may significantly affect the ignition performance of the exposed surface. Increasing the thermal capacity of the underlying construction increases the "heat sink" effect and may delay ignition of the exposed surface. Any backing provided to the test specimens and in intimate contact with them, such as the baseboards, may alter this "heat sink" effect and may be fundamental to the test result itself.

With thin materials or composites which in practice may be used with a variety of substrates, it may be advisable to carry out tests with several types of substrate to obtain an indication of the likely ignition performance in practice. Both the "thermal inertia"(related to the product of thermal conductivity, density and specific heat) of the substrate and its combustibility may affect the ignition performance of the material or composite.

**A.4.2** Further development work will be needed before problems associated with some unusual specimens can be resolved. For example, a thin specimen of material which is normally backed by air should be tested with as realistic an air gap as possible.

It is possible that in some circumstances the use of a closed cavity in representing an air gap could create problems.

**A.4.3** Constant mass is proof of satisfactory conditioning; cellulosic materials may require periods in excess of two weeks to reach equilibrium with the conditioning atmosphere, but plastics may take less time. Unless otherwise specified in established standards, each test specimen of plastics should be conditioned for at least 48h at  $(23 \pm 2)^{\circ}\text{C}$  and  $(50 \pm 5)\%$  RH (see ISO 291) immediately prior to use.

## A.5 Test set-up

**A.5.1** Three methods have been found suitable for the attachment of the thermocouples to the heater coil.

- a) A type K (Ni-Cr/Ni-Al) or type R (Pt/Pt 13% Rh) thermocouple in a 1mm diameter stainless steel sheath, capable of continuous operation at 900°C, with insulated hot junction, is inserted as a "push fit" in a hole in a stainless steel block brazed to the heater element with an alloy having a remelt temperature of more than 900°C (see figure 4c).
- b) A type K or R thermocouple in a 1mm diameter stainless-steel sheath, capable of continuous operation at 900°C, with insulated hot junction, is held in contact with the heater element by means of a small stainless-steel clamp (see figure 4c). The clamp is tightened by pinching the projecting lug with pliers.
- c) A type K insulated and glass-braided thermocouple having 0,5mm diameter wires individually welded to the heater element. The thermocouple junction is formed by welding the individual wires to the heater element approximately 3mm apart by a capacitor discharge welder (see figure 4c).

Both the clamp and the block should be roughened with emery paper and the heater run for several days at a temperature of 600°C to 700°C before calibration of the apparatus to encourage stabilization of a high emissivity. Until it is clear that stabilization has occurred, a new heater coil should be calibrated more frequently than is required in 10.3.

The thermocouples may be inserted through the upper or lower apertures of the radiator cone, or through a hole in the shade. The thermocouples shall be securely held close to their entry into the radiator core.

**A.5.2** The mechanism for the pilot flame application in figures 2 and 6 can give the specified application time for the flame of  $t_0^{+0.1}$  s when the surface of the specimen remains dimensionally stable. If, however, the specimen swells and the surface rises, the application time will increase and, if the specimen shrinks downwards, the application time will decrease. It is thought that this should be accepted for the present, and only if experience shows it to be necessary should a mechanism be developed which will maintain an application time of  $t_0^{+0.1}$  s irrespective of surface movement. For the mechanism recommended, the variation of application time with position of surface will be reproducible between different types of apparatus.

The flow rates specified in 9.2 should give a pilot flame about 10mm long.

**A.5.3** Whilst phase angle control is allowed for the temperature controller of the radiator cone, it should be noted that this will usually require electrical filtering to avoid noise on low-level signal lines.

## A.6 Test procedure

**A.6.1** A convenient way of setting the counterweight mechanism to give the force of approximately 20N, as required by 11.1, between the pressing plate and the masking plate, is to use the pivoted counterweight arm as a balance. If a 2kg mass is temporarily suspended from the underside of the opposite end of the pivoted arm from the counterweight, the counterweight can then be set to produce a balance either by adding extra, removable, weights to it or by adjusting its position on the pivoted arm. The 2kg mass can then be removed, hence giving the correct force on the bottom of the sliding rod which operates the pressing plate. Alternatively, the position of the counterweight on the pivoted arm could be calibrated against the mass of the specimen.

**A.6.2** When testing more than one material at a time, it may be convenient and more expedient to continue tests at the same irradiance on another batch of five specimens prior to changing the irradiance setting of the apparatus. In this case it will be necessary to readjust the counterweight before each set of specimens.

**A.6.3** Once ignition of a specimen has occurred, it should be extinguished as soon as possible to prevent excessive cooling of the radiator cone by the increased airflow through it. In between successive specimens, it is necessary to ensure that a sufficient time interval is left to allow the apparatus to reach equilibrium.

Attainment of temperature equilibrium of the heater is shown by the indicating meter and, once this is obtained, a further period of not less than 3 min should elapse before the next test to ensure that the remainder of the apparatus has attained sufficient temperature equilibrium. This procedure, with a delay period of 3 min, is also applicable for a change in irradiance.

**A.6.4** Careful observation of the behaviour of the surface of the specimen and the action of the pilot flame as it comes to the surface should be made. If the adjustable stop on the travel of the pilot flame application mechanism has to be used, it may require constant adjustment between subsequent applications of the pilot flame.

**A.6.5** To avoid disturbance to the ambient air flow, it is recommended that the operator should avoid excessive sudden movements.

## **A.7 Safety**

A safety warning is given before the Scope relating to the evolution of toxic or harmful gases during the exposure of test specimens. Attention should also be drawn to the hazards arising from the hot radiator cone, the use of a mains voltage electricity supply and the use of water to extinguish and cool down specimens after ignition. The possibility of the violent ejection of molten hot material or sharp fragments from some kinds of specimens when irradiated cannot totally be discounted and eye protection should be used by the operator.

## **Annex B** (informative)

### **Application and limitations of test**

The test method specified in this International Standard is concerned with essentially flat building products (materials, composites or assemblies) which may be exposed to fire and whose ignition and subsequent burning may affect fire growth and spread. The test examines the ability of products to become ignited when irradiated from a primary fire in the presence of means for piloting the ignition. In practice this might be by flame contact, continuous or intermittent, or by embers, sparks or by burning material falling down.

It is one of a series of tests for the reaction to fire being developed by ISO/TC 92, the results of all of which will usually need to be considered together in order to assess the effect of such products on fire behaviour and hence to enable requirements for building control to be specified.

The test is intended to provide information which can be used in the evaluation of wall and ceiling linings, flooring systems, external claddings, and duct insulation materials. In some well-defined circumstances the exposure to fire of such products is capable of precise specification and the result of the test may be directly related to the performance expected in practice. In other cases a much less precise specification will be possible. However, the test may be made use of to distinguish products which are more easily ignited from those which are less easily ignited; this will often contribute to a difference in hazards between the materials.

The method may also be applicable to non-building products.

Evidence is accumulating for a correlation between the ignitability test specified in International Standards and flame spread tests, at least for the higher flux levels. It is possible that the results of the ignitability test could provide a good measure of fire growth.

The present test does not consider the ability to ignite by flame contact alone, without additional impressed radiation.

The test uses a horizontal specimen, but this is rather to permit the testing of thermoplastics than to represent products which in practice are used in a horizontal orientation. In any case, the representation of the ignition of realistic exposed areas of vertically orientated products is not necessarily achieved simply by a test with a small vertical specimen. The orientation will affect other variables which in turn can modify time to ignition, for example, the absorption of radiation in the volatiles being generated by the specimen and the modification of the air flow past the specimen by the heater. Orientation and specimen size may well interact.

The test will have particular relevance for fire initiation, spread and growth situations where, once a fire has grown to a certain point, a new phase of spread or growth is possible if ignition by radiation can bring fuel hitherto uninvolved into play. For example, a relatively small fire near a wall in a compartment may be expected to grow rapidly if it succeeds in igniting a flammable wall lining; ignition of a lining material in a corridor heated by strong radiation passing through a door opening from a well-developed fire in a room may initiate a phase of fire spread in the corridor.

Ignition by radiation is clearly an important consideration where protection against fire spread is being sought by spatial separation (for example spread of fire between buildings can be prevented by spacing them sufficiently apart). The ignition performance of modern materials is a factor of especial importance

here since existing building control for space separation has as an underlying basis the critical irradiance for pilot ignition essentially of cellulosic materials.

One feature of the test is that the specimens are heated almost entirely by radiation. The ignition performance of a specimen with a shiny metallic finish might be much better in this test than it would be in practice in a situation where, by contact with the flame or combustion gases, the absorptance of the finish may be markedly increased by soot deposition or condensation of moisture. It should be realised that the visual appearance of a surface is not always a guide to its absorptance for thermal radiation. White surfaces, with low absorptance for white light may have high absorptance for thermal radiation from sources at fire temperature.

**Annex C**  
(informative)

**Higher heat flux capabilities**

Studies have been carried out to determine the feasibility of using the apparatus specified in this International Standard at higher heat flux levels than those stated. Extensive studies on a large variety of materials have shown that products can be assessed by routine operation of the apparatus up to the 70kW/m<sup>2</sup> level given in this method. In addition, work has also shown that the apparatus can be operated at higher heat flux levels. The heater can operate to provide a stable output yielding irradiances of 75 to 95kW/m<sup>2</sup> for periods of up to 6 hours.

At a heat flux of 100kW/m<sup>2</sup>, a slight fluctuation in the measured irradiance has been observed with current designs of apparatus, over a 7-hour period. The heat flux recorded varied between 100 and 102kW/m<sup>2</sup>, with the tendency towards a slightly upward drift.

Table C.1 gives an indication of the temperatures which provide heat flux levels of between 70 and 100kW/m<sup>2</sup>.

**Table C.1 — Temperature required to obtain heat fluxes**

<b>Heat flux</b> kW/m <sup>2</sup>	<b>Approximate temperature controller setting</b> (°C)
70	890
75	905
80	915
85	930
90	950
95	965
100*	980

\* Slight drift in value was observed.

## Annex D (informative)

### Interlaboratory trial on variability in time to sustained surface ignition

An interlaboratory trial was carried out in which replicate batches of five materials were tested by six laboratories according to the test procedure given in this International Standard.

No significant differences in ignition time, were found within the laboratories. The interlaboratory trial did, however, show that the sustained surface ignition times of some materials were relatively more variable than those of others. Furthermore, for some materials the relative variability increased with decreasing irradiance. It is therefore not meaningful to quote a single value for the variation of the test.

No significant differences in the variability of the time to sustained surface ignition were found between the participating laboratories, but ignition time is sensitive to irradiance and it became clear during the trial that careful attention must be paid to the measurement of irradiance and the calibration of the apparatus.

Table D.1 gives the results of the statistical analysis of results in terms of the mean, repeatability and reproducibilities, expressed both in seconds and as a percentage of the mean in order to facilitate the examination of results, defined in accordance with ISO 5725-1.

Repeatability ( $r$ ) is the value below which the difference between two ignition times obtained with the same method on identical test material, under the same conditions (same laboratory, same apparatus, same operator, and a short interval of time), may be expected to lie within a specified probability (in this case taken as 95%).

Reproducibility ( $R$ ) is the value below which the difference between two ignition times obtained with the same method on identical test material, under "different" conditions (different laboratories, different operators, different apparatuses and/or different times), may be expected to lie with a specified probability (in this case taken as 95%).

The values in table D.1 suggest that for some products there is relatively greater variation at a lower irradiance.

Table D.1 — Repeatability and reproducibility data for time to surface ignition

Products	Poly(methyl methacrylate)		Medium density fibreboard		Poly(vinyl chloride)-coated steel plate		Gypsum plasterboard		PVC	
<b>Thickness</b>	10 mm		12 mm		200 µm		9,5 mm		2 mm	
<b>Heat flux (kW/m<sup>2</sup>)</b>	30	40	30	40	30	40	30	40	30	40
<b>No. of laboratories</b>	5	5	5	5	7	7	6	7	7	7
<b>Mean, in s</b>	78,5	44,7	85,7	48,3	29,7	20,5	128,0	57,7	138,4	44,9
<b>Repeatability (r), in s</b>	7,2	4,4	10,3	8,3	6,2	4,4	15,7	8,8	50,7	4,5
<b>% of mean</b>	9,2	9,9	12,1	17,3	20,8	21,3	12,3	15,2	36,6	10,1
<b>Reproducibility (R), in s</b>	19,1	10,4	18,2	13,5	8,1	6,0	33,2	19,4	74,8	8,2
<b>% of mean</b>	24,4	23,2	21,2	27,9	27,2	29,0	25,9	33,6	54,0	18,2



**Annex E**  
(informative)

**Bibliography**

- [1] ISO/TR 3814:1989, *Tests for measuring "reaction to fire" of building materials – Their development and application.*
- [2] ISO 5725-1:1994, *Accuracy (trueness and precision) of measurement methods and results – Part 1: General principles and definitions.*
- [3] ISO/TR 6585:1979, *Fire hazard and the design and use of fire tests*<sup>3)</sup>.
- [4] KASHIWAGI, T. Experimental Observation of Radiative Ignition Mechanisms. *Combustion and Flame*, **34**, 1979, pp. 231-244.

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<sup>3</sup> Now withdrawn.